



Final Report

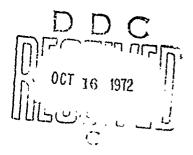
Final Report

June 1972

PARAMETRIC STUDY OF THERMAL PROBLEMS IN DENSELY POPULATED SHELTERS

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heat from human bodies to a shelter environment and to some effects of population density on optimum clothing, skin wetness, limits for thermal equilibrium, and contributions made by each of six processes for heat/mass transfer. These processes include: radiation and convertion at skin or clothing surfaces, heat conduction through clothing, respiratory heat exchange, vapor diffusion through dry skin, and evaporation of sweat at wet skin surfaces. Thermal equilibrium is maintained in cool environments by modifying thermal resistance of clothing and in warm environments by adjusting the ratio of wet to total skin areas. Also, an analysis of moist-air mixing processes is used to evaluate operational requirements for partial recirculation of ventilating

air during cold weather. Analyses and computations are based on correlated data from

Thermal problems treated analytically in this report relate to transfer of metabolic

the scientific literature. Results are presented graphically in 9 figures and numerically in 18 tables.

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Survival									
Thermal environment									
Thermal problems									
Population density									
Environmental control									
Metabolic heat									
Thermal equilibrium									
Temperature									
Humidity									
Radiation									
Convection									
Evaporation									
Insensible weight loss									
Clothing									
Heat transfer									
Ventilation									
Air distribution									
Psychrometric process									
Partial recirculation									
Air mixing									
Cold weather									
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SUMMARY

Introduction

The problems investigated in this study relate to the effects of population density on the transfer of metabolic heat and assisture from sedentary persons to the environment in shelters. Also, parameters associated with nonuniform (varistate) environments and partial recirculation of ventilating air during cool or cold seasons are evaluated.

Metabolic Heat Transfer

To maintain deep-tissue and skin-surface temperatures within ranges compatible with acceptable levels of comfort, the human body must reject heat to the environment by one or more physical processes in accordance with equations for thermal equilibrium,

$$S = M - W - (R_s + C_s + C_r) - (E_w + E_d + E_r) = 0$$

in which quantities are energy rates, as follows:

- S = heat storage (positive if mean body temperature tends to increase)
- M = metabolic energy expenditure (100 kcal/hr for a sedentary person having a skin surface area of 2 square meters)
- W = external work performed (zero for sedentary persons)
- R_s = heat transfer by radiation at exposed surfaces of skin or clothing
- C_s = heat transfer by convection at exposed surfaces of skin or clothing
- C_r = heat associated with change in temperature of respired air
- E_{w} = heat transfer by evaporation of sweat at wet skin areas
- E_d = heat transfer by diffusion of water vapor through dry skin
- E_r = heat of vaporization associated with moisture added to respired air.

The components of sensible heat, $(R_s + C_s + C_r)$, and latent heat, $(E_w + E_d + E_r)$, are positive if the process tends to cool the body.

Each of the heat transfer processes has been evaluated, together with appropriate coefficients, by reference to scientific literature, and the results are used to synthesize a program for computing metabolic parameters under selected conditions. The program is based on maintenance of model skin temperatures under all combinations of conditions for which thermal equilibrium is possible by varying either the insulating value of clothing or the evaporative cooling effect associated with sweat gland activity. The threshold for regulatory secretion of sweat corresponds to the temperature at which the required insulating value of clothing is just zero. At higher temperatures, sweat rates and skin wetness are increased to develop the required evaporative cooling effect. A limit for thermal equilibrium is reached when either the skin is completely wet or a maximum sweat rate is attained. Within an air temperature range of 10°C (50°F) to 52°C (125.6°F), model skin temperatures for sedentary persons vary from 32°C (89.6°F), at which skin is typically dry, to 36°C (96.8°F), at which skin may be completely wet in a humid environment.

Computed values of metabolic data relating to sedentary persons are tabulated in the report for the nine combinations of conditions listed in Table S-1. For each of nine values of air temperature and three values of relative humidity, the numerical tables include the following items of metabolic data:

- · Saturated vapor pressure at mean skin temperature
- Latent heat transfer
- · Sensible heat transfer
- Heat storage

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- Heat transfer by radiation at exposed surfaces
- Heat transfer by convection at exposed surfaces
- · Sensible heat transfer associated with respiration
- · Latent heat transfer associated with respiration
- · Latent heat transfer by vapor diffusion through dry skin
- · Latent heat transfer by evaporation at wet skin areas
- Partial pressure of water vapor in the environment
- Thermal resistance of clothing needed for thermal equilibrium 1.
 cool environment
- Ratio of wet to total skin areas

TABLE S-1

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DATA FOR NUMERICAL TABLES OF METABOLIC PARAMETERS

						<u> </u>			
TABLE NUMBER	A-2	A-3	A-4	A-5	A-6	A-7	A-8	A-9	A-10
SKIN TEMPERATURE, T3, AT AIR TEMPERATURE, T, (CELSIUS) T3=34 T3=34+1.5*ATN(0.1967*(T-31))	×	×	×	×	×	×	×	×	×
ATTENUATION FACTOR, F3, FOR VAPOR DIFFUSION THROUGH CLOTHED SKIN AREAS F3=1.0 F3=1.(1+0.1%K2) F3=1/(1+0.2%x2)	×	×	×	*	×	×	×	×	· ,
MEAN RADIANT TEMPERATURE, T1, IN OCCUPIED SPACE (CELSIUS) T1=T T1=T3 OR T1=T2 T1=(T3+T)/2 OR T1=(T2+T)/2	×	×	×	×	×	×	×	×	< ×
CONVECTION COEFFICIENT, HI, FOR EXPOSED SKIN OR CLOTHING KCAL/(HR#SQ M#oc)	4.0	4.0	4.0	3.4	5.0	7.0	4.0	. 4	0.4
EVAPORATION COEFFICIENT, E1, FOR WET SKIN AREAS KCAL/(HR*SQ M**MMHG)	8.0	8.0	8.0	6.8	10.0	14.0	8.0	0 . 8	3. 8
RELATIVE AIR VELOCITY, VI CENTIMETERS/SECOND FEET/MINUTE	15	12.0	15	10	23	45 90	15	15	15 30

(CELSIUS) T3=SKIN TEMPERATURE, T2=CLOTHING TEMPERATURE, T=AIR TEMPERATURE K2=THERMAL RESISTANCE OF CLOTHING (CLO UNITS)

· Temperature gradient through clothing.

Relationships among metabolic parameters are illustrated graphically in the report by Figures 4, 5, and 6, which are based on conditions shown for Tables A-3 and A-4 in Table S-1.

Effects of Population Density

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If ventilating air is supplied to an unoccupied, insulated room through openings at one end and removed through openings at the opposite end, temperatures and longitudinal air velocities in the space should be virtually uniform, and the mean radiant temperature should be equal to the air temperature. The entry of people into this room would divert air to levels near the ceiling because people partially obstruct air flow near the floor level. If the population becomes dense and overhead clearance is relatively large, most of the air may flow through the overhead space. Air velocities near the floor may then approach the low values associated with natural convection, and coefficients for transfer of metabolic heat and moisture would be proportionately reduced. The increase in population density would also cause a change in mean radiant temperature to a value that is intermediate between mean wall surface temperature and the mean temperature of exposed skin or clothing surfaces. The magnitude of these effects is closely related to quantities that are evaluated in the study of metabolic parameters under the conditions listed in Table S-1. Tabulated values of relative air velocity include 20, 30, 45, and 90 feet per minute. Values are tabulated at an air velocity of 30 feet per minute with mean radiant temperatures that are:

- Equal to air temperature
- · Equal to the temperature of exposed skin or clothing surfaces
- The mean of air temperature and the temperature of exposed skin or clothing.

Shelter Ventilation

When ventilating air is well distributed in accordance with the distribution of heat loads in an occupied space, the environment may approach spatial uniformity. On the other hand, if the ventilating air moves horizontally through the space from one boundary to an opposite boundary, environmental conditions will change gradually as metabolic heat and moisture are added along the air stream. The environmental temperature adjacent to the boundary along which air is supplied to the space will be essentially

the same as the supply air temperature. If the ventilating system supplies only atmospheric (outside) air to the space, shelter temperatures during wintertime may be warm at the end from which air is exhausted, but may be far below the prescribed minimum of $50^{\circ}F$ near the end to which air is supplied. This study demonstrates that a minimum temperature of $50^{\circ}F$ in the occupied space of a shelter that has insulated or massive walls can be maintained during very cold weather by partial recirculation of ventilating air, a mixing process that utilizes metabolic heat for tempering fresh air.

Ventilation process lines, each of which shows the locus of environmental states along a path of air flow, are determined on the basis of a pair of linear equations that approximate metabolic data derived in the section on Metabolic Parameters. These equations are:

 $\rho = 0.25$ when $T \leq 82.5^{\circ}F$

and

 $\rho = 0.06T - 4.7$ when $T \ge 82.5^{\circ}F$

where

 ρ = ratio of latent to total metabolic heat T = air temperature of local environment.

Several ventilation process lines, each of which approaches the value $T = 95^{\circ}F$ asymptotically, are shown graphically on Figure 7 in the report. This figure also includes isoventilation lines that relate the temperature of exhaust (or recirculated) air to ventilating rate, when fresh or mixed air is supplied to the occupied space at a temperature of $50^{\circ}F$.

A computer program that simulates the process for mixing fresh and recirculated air was developed on the basis of a nonuniform environment and used to evaluate parameters associated with the partial recirculation process when the mixed (supply) air temperature is $50^{\circ}F$ and the fresh air temperature varies from $+50^{\circ}F$ to $-50^{\circ}F$. The results are shown graphically on Figure S-1 and numerically in Appendix B of the report.

The effects of heat transmission through building elements on surface temperatures, interactions among metabolic parameters, partial recirculation of air, and the configuration of ventilating systems should be investigated in depth.

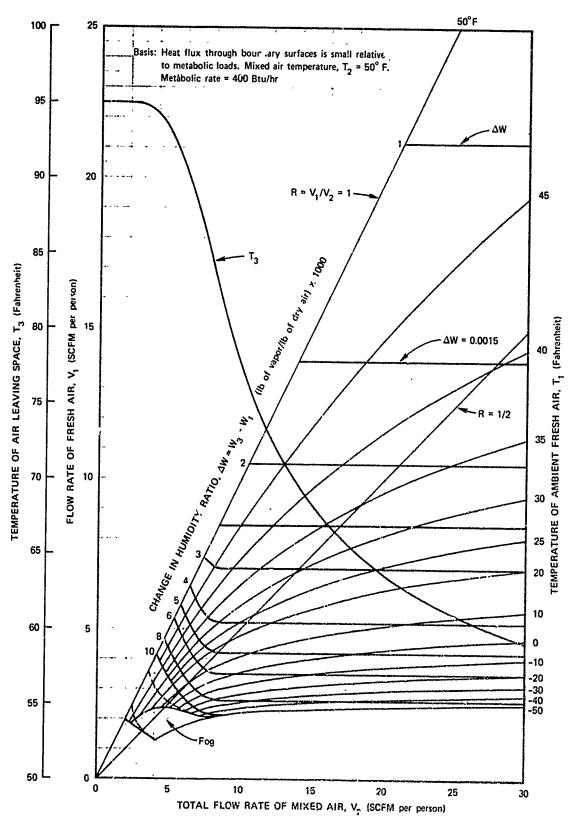


FIGURE S-1 . VENTILATION OF AN OCCUPIED SPACE WITH MIXED FRESH AND RECIRCULATED AIR AT 50°F

ABSTRACT

The thermal problems considered in these studies are associated with the transfer of metabolic heat and moisture from the human body to a shelter environment and with the effects thereon of population density. The studies are also concerned with the requirements and rationale for partial recirculation of ventilating air in shelters during cool and cold weather.

An analytical model for thermal metabolism is developed and used to evaluate metabolic parameters under several conditions of shelter occupancy. This model includes the effects of six processes for transfer of metabolic heat: radiation at skin or clothing surfaces, convection at skin or clothing surfaces, heat conduction through clothing, respiratory heat exchange, vapor diffusion through dry skin, and evaporation of sweat from wet skin surfaces. Thermal equilibrium is maintained in cool environments by modifying the thermal resistance of clothing, and in warm environments by adjusting the ratio of wet to total skin surface, that is, the rate of evaporative cooling. The parameters are correlated graphically, and supplementary data are included in numerical tables.

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Ventilation process lines for varistate environments are shown on a psychrometric chart, together with isoventilation lines for an initial or mixed air temperature of 50° F, as supplied to the shelter. Parameters associated with partial recirculation of air when ambient conditions are less than or equal to 50° F are compared graphically.

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INTRODUCTION

If a shelter or other occupied space is to remain habitable, means must be provided for maintaining an environment that is capable of supporting essential metabolic processes. Thus, oxygen consumed must be replaced, excessive concentrations of carbon dioxide and other noxious constituents must not be allowed to develop, and the transfer of metabolic heat and moisture to the environment must be possible with near-normal body temperatures. In general, elementary control of a shelter environment can be accomplished most economically by ventilation with air from the surrounding atmosphere.

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Per capita ventilating rates required to maintain an environment in which the effective temperature is equal to or less than a stated value during at least a stated percentage of the hours in an average year have been determined for shelters in various climatic locations. Criteria based on these determinations have been promulgated for application to shelters; these criteria specify that effective temperatures in occupied shelters shall be 82° FET or less during at least 90 percent of the days in an average year. It is further specified that the minimum temperature in a shelter environment shall not be less than 50°F. Capacities of ventilation systems determined under these criteria vary from 5 SCFM per person in Alaska to 40 SCFM per person along part of the Gulf coast of Texas. These criteria are based on analyses in which the environment is assumed to be spatially uniform. Air envering an occupied space is

References are listed at the end of the report

The unit SCFM refers to standard cubic feet per minute, that is, air having a dry density of 0.075 lb/ft³.

assumed to mix completely and instantaneously with air in the space. The shelter structure is assumed to be perfectly insulated or "adiabatic."

Assumption of a uniform environment is consistent with air conditioning practice, in which air is usually well distributed within occupied spaces by a system of ducts and diffusion outlets. A more realistic assumption for the case of shelters would be that air will not be distributed in proportion to heat loads, but that heat and moisture will be added gradually to air stream as it passes through occupied spaces—in particular, through large, densely-populated spaces. Some effects of this gradual addition of heat and moisture to ventilating air have been demonstrated experimentally in the monoman calorimeter, and analytically in a study of ventilating and mixing processes in shelters.

Studies documented herein are concerned with the reciprocal effects of population density in a shelter on the thermal environment and the physical processes for transfer of metabolic heat from the human body to its surroundings. The studies include the derivation of a set of quantitative requirements for seasonal recirculation of ventilating air in shelters. Problems associated with population density stem from the facts that human bodies obstruct the normal flow of ventilating air and change the mean radiant temperature within an occupied space. These effects usually interfere to some degree with transfer of metabolic heat and therefore tend to modify the effective temperature or other index of environmental habitability. A meaningful study of these problems can only be made in conjunction with an evaluation of all significant physical processes for transfer of metabolic heat and moisture and the physiological reactions that can control these processes. The usual partition of metabolic heat into sensible and latent fractions is not sufficient for the purpose. A major effort has therefore been devoted to development of an analytical model for metabolic interactions with the environment.

II METABOLIC PARAMETERS

Seasonal and spatial variations in temperature may be relatively large if an occupied shelter is ventilated with outside air and no apparatus is provided for supplementary heating or cooling. Temperatures in occupied spaces may rise to $100^{
m O}$ F or more during warm seasons or fall to 50°F or less during cold seasons. To maintain a tolerable degree of comfort throughout this wide range of environmental conditions, clothing that is adapted to the prevailing condition must be worn. Thus, heavy or multilayered clothing would be optimum when the temperature is 50°F, and light (or no) clothing would be optimum during hot weather. This situation is not adequately represented by metabolic data for nude and clothed persons in technical literature in which the term "clothed" implies clothing that is suited to normal room temperatures. Thus, at lower temperatures, the data include either a large storage component or a high metabolic rate to obtain a heat balance. Moreover, published data evaluate only the sensible and latent components of metabolic heat. Such data do not provide information on the relative contributions made to thermal equilibrium by radiation, convection, and the several modes of evaporation.

For almost 50 years, the effective temperature index (ET) has served as a means for evaluating habitability of an environment. This index, which considers the effects of temperature, humidity, and air motion, was determined empirically from subjective responses of persons during short exposures in test environments. In 1947, Yaglou suggested that mean skin temperature could be used as an index of comfort. Since that time there has been a continuing effort to devise a comprehensive index of comfort based on measurable physiological quantitites. This

effort has led to a better understanding of processes and control mechanisms for transfer of metabolic heat and moisture, and has resulted in the development of several methods for evaluating environments with regard to human comfort. Recent investigators have defined rational relationships for the diffusion of water vapor through dry skin, a process that has been controversial since Sanctorius first measured weight loss associated with insensible perspiration in the seventeenth century. Evaluation of this diffusion process and the process for latent heat transfer in the respiratory tract are of special interest in connection with the present study because these phenomena should be sensitive to changes in environmental humidity. Earlier sources of metabolic data have indicated that humidity has no significant effect on the partition of metabolic heat. 19,16-18

For the purposes of this study, empirical expressions that define six processes for transfer of metabolic heat and moisture are evaluated by reference to technical and scientific literature to establish a reasonable level of confidence in the results. These expressions are then used to synthesize a computer program for calculation of combined effects and resultant parameters. The six contributory processes are as follows:

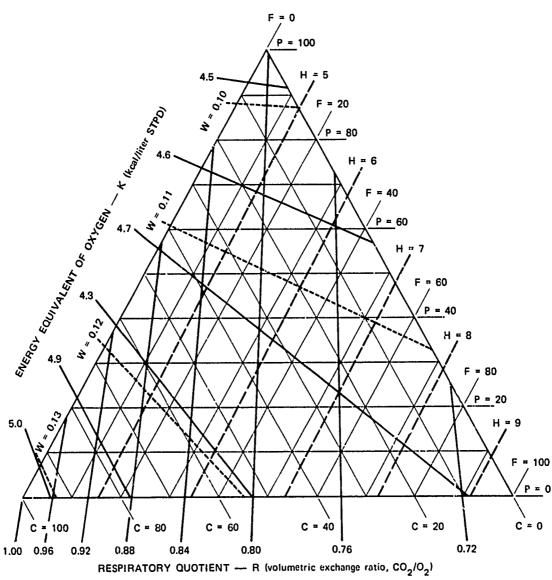
- Heat and moisture transfer in the respiratory tract
- Vapor diffusion through dry skin surface
- Evaporation of sweat from wet skin surfaces
- · Convection from exposed surfaces of skin or clothing
- Radiation from exposed surfaces of skin or clothing
- · Heat conduction through clothing.

Insofar as possible, data from original sources are interpreted and reduced to a common denominator in accordance with definitions and procedures outlined in recent biological handbooks.

Most of the available data on energy expenditure, work capacity, and pulmonary ventilation is based on indirect calorimetry; that is, metabolic rates are deduced from measurements of breathing volume, temperature, pressure and changes in oxygen and carbon dioxide concentration during respiration. A value of 4.825 kilogram calories per liter of oxygen consumed is often used for this purpose. 19 However, the true energy equivalent for oxygen varies with the respiratory quotient (RQ), which is the volumetric ratio of carbon dioxide produced to oxygen consumed. The normal range of variation for this energy/oxygen equivalent can be illustrated by constructing a triaxial graph based on a set of linear equations derived by MacHattie. 21,22 This graph, which is shown in Figure 1, has three coordinate scales to represent the composition of a mixture of metabolized nutrients; that is, percentages of typical carbohydrates, fats, and proteins. Curves for other parameters are superimposed on this triaxial grid and are identified in Figure 1. According to Weir, an average diet will result in metabolism of 10 to 15 percent of proteins with an RQ of about 83 percent. The energy equivalent for oxygen, K, would then be slightly more than 4.8 kilogram calories per liter of oxygen, STPD. * Under STPD conditions, oxygen has a density of 1.4277 grams per liter, or 0.08915 pounds per cubic foot. 24 The parameters evaluated in Figure 1 are typical for normal subjects engaged in sedentary activities, but may not be representative for persons having metabolic disorders (such as diabetes) or persons engaged in strenuous activities. Severe exercise and the onset of muscular

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The abbreviation STPD refers to the standard volume of a gas measured in the dry state at a pressure of one atmosphere and a temperature O°C. Breathing volumes are usually measured in the expired ATPS state, but reported in the BTPS state. ATPS refers to a volume of air in the saturated state at ambient temperature and pressure; BTPS refers to a volume of air in the saturated state at normal body temperature and ambient atmospheric pressure.



C, F and P are, respectively, the percentages of carbohydrate, fat and protein metabolized in a mixture of these fuels H is caloric value of the metabolized mixture (kcal/gram).

W is quantity of metabolic water produced (grams/kcal).

Based on data from Reference 21.

FIGURE 1 BASIC PARAMETERS ASSOCIATED WITH ENERGY METABOLISM

fatigue are characteristically accompanied by the formation of blood lactates and an RQ greater than unity. With regard to the storage of drinking water in shelters, it is interesting to note that the metabolic process produces about 0.12 grams of water per kilogram calorie of energy expenditure. For a man having an average metabolic rate of 75 kcal/hr, this is about 0.48 lb/day or 0.057.gal/day.

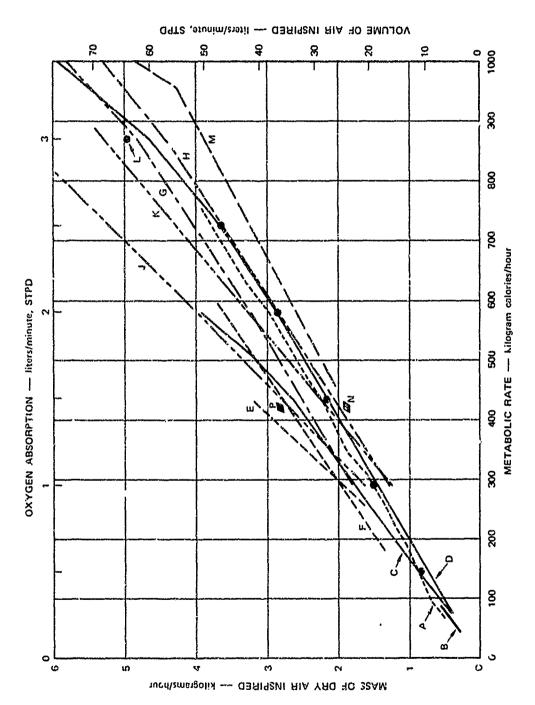
Respiratory Heat Exchange

Volume and Mass of Inspired Air

Respiratory heat exchange includes a sensible heat fraction (identified with the difference between the temperatures of inspired and expired air) and a latent heat fraction (associated with the change in moisture content of respired air). The magnitude of both effects is proportional to the rate of pulmonary ventilation, which in turn is proportional to the rate of energy expenditure or the oxygen consumption. Experimental data from nine sources are plotted in Figure 2. These data have been reduced to the STPD condition and converted from the expired to the inspired state, as necessary. A respiratory quotient of 85 percent was assumed in treating data that did not include values for this parameter. For the purpose of evaluating respiratory heat exchange, an equation that relates the inspired mass of dry air to the metabolic rate will be convenient.

In Figure 2, Curve A (dashed) represents data from a series of tests reported in 1912 by Douglas and Haldane in which one subject (Douglas) walked in the laboratory and on grass at speeds of 2 to 5 miles per hour. Curve B (short lines) represents average values from basal metabolism tests made by Boyer and Bailey of 500 normal subjects. Curves C and D (solid lines) represent data from Asmussen and Nielsen for activities in which arm action (Curve C) or leg action (Curve D) is predominant. The increased pulmonary ventilation associated with arm





RELATIONSHIP OF PULMONARY VENTILATION TO ENERGY EXPENDITURE FIGURE 2

motion is ascribed to mechanical manipulation of the rib cage. Curves E and F (dashed lines) represent data from Liddell for mining tasks that involve arm action (Curve E) and walking tasks (Curve F). 29 Curves G, H, J, and K (broken lines) represent data from Hermansen and Saltin. 30 Curves G and H are for trained athletes exercising on a bicycle ergometer (Curve G) or a treadmill (Curve H). Curves J and K are for untrained students exercising on a bicycle ergometer (Curve J) or a treadmill (Curve K). The trained athletes can extract more oxygen from a given quantity of air. Curve L (heavy dots) represents a series of tests for one subject exercising on a bicycle ergometer, first in the normal upright position and then while seated in an easy chair in a reclining position. 31,32 The results in these two positions were virtually identical. Curve M is the lower boundary of plotted data from 611 tests with 86 subjects, as reported by 11 investigators. 33 These tests involved walking, running and bicycling. The upper boundary of the data would interfere with identity of curves C, J, and F. Lines through the origin and the diamonds, N and P, would represent values of 2.0 and 3.0 for the "ventilatory equivalent for oxygen." This quantity can be defined numerically as the number of liters of air expired in the BTPS state for each 100 cubic centimeters of oxygen used in the STPD state. 19 In general, the ventilatory equivalent for oxygen associated with healthy persons engaged in normal activities will remain within the range of 2 to 3. to Knipping and Moncrieff, 34 lower values are characteristic for sleeping persons, and higher values may be associated with nervous tension or with the presence of such health disorders as heart disease, diabetes, anemia, and tuberculosis.

On the basis of data in Figure 2, a reasonable approximation for the mass of dry air inspired by people in shelters is

$$G = 0.006M \tag{1}$$

where

The second secon

G = mass of dry air inspired (kilograms/hr)

M = metabolic rate (kilogram calories/hr).

If the subjects are athletes and the activity involves little or no arm motion, G=0.005M may be a better approximation. Equation (3) is used in subsequent computations relating to respiratory heat losses and shelter ventilation. The mass velocity of dry air inspired by a sedentary individual having a metabolic rate of 100 kcal/hr (397 Btu/hr) is therefore 0.60 kg/hr (1.32 lb/hr).

Properties of Respired Air

To evaluate the contribution made by respiration in the transfer of metabolic heat and moisture, a logical relationship between the properties of inspired and expired air must be educed from the mass of literature relating to insensible weight loss or insensible perspiration. Insensible weight loss includes the moisture loss by diffusion through dry skin, the moisture added to respired air, and the differential mass associated with oxygen uptake and carbon dioxide rejection. For the purposes of this study, the experimental data and supporting information developed by Cole are most useful.

Cole's data were obtained with subjects breathing either dried air or air saturated with moisture at temperatures of -30°C to +50°C. On the basis of his investigations, Cole derived several conclusions that are pertinent to this study, as follows:

- Saturated air inspired at body temperature (37°C) is expired in the same condition.
- Air in the lungs is saturated with water vapor at body temperature.
- The upper respiratory tract serves as an efficient device for heat recovery. For example, during inspiration of co.d air,

surfaces of the upper respiratory tract (nasal mucosa) are chilled. During expiration, these chilled surfaces are warmed by heat and moisture extracted from the expired air.

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 The condition of expired air is independent of the rate of pulmonary ventilation.

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- Within terrestrial limits, changes in altitude have little effect upon the condition of respiratory air.
- The body loses more heat and moisture during oral than during nasal breathing at room temperature.
- During nasal areathing, remote thermal stimuli can modify blood flow to nasal mucosa and raise or lower the temperature of inspired air in the pharynx and expired air at the anterior nares. A comparable effect is not exhibited during oral breathing. For example, during nasal breathing at room temperature, immersion of the feet in warm water at 45°C is accompanied by an increase of 2°C to 3°C in the temperature of expired air. Local heating (or cooling) of the dorsal region of the back is also accompanied by an increase (or decrease) in expired air temperature.

Cole's conclusions were generally confirmed by Ingelstedt. The recovery of heat in the upper respiratory tract was well demonstrated by Seeley. The temperatures of expired air indicated by Cole are in good agreement with values obtained by Seeley and Webb, the are generally lower than data at moderate and high termperatures obtained by Burch and McCutchan and Taylor. The experimental procedures of both Burch and McCutchan and Taylor were based on oral breathing, and the expired air was usually found to be less than saturated. In analyzing data on heat removed from the body by respiration, Burch included the effect of decomposition of carbonic acid. An analysis of heat exchange by Caldwell,

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Gomez, and Fritts shows that this endothermic reaction is counteracted by an exothermic effect arising from the combination of oxygen with blood.

Figure 3 shows a model for respiratory parameters associated with a wide range of environmental conditions. Within the range of inspired air temperatures extending from -30°C to ±50°C, the solid lines labeled 0% and 100% are a good representation for Cole's data. The curves are extrapolated below and above this range. It is assumed that expired air temperatures associated with inspired air having relative humidities between 0 and 100 percent can be determined by linear interpolation. Therefore, in accordance with Cole's postulate that expired air is virtually saturated, the two solid curves on Figure 3 completely define the condition of expired air associated with any given condition of inspired air within these wide limits. With reference to Figure 3, the equation for expired air temperature is

$$T_e = U_0 + \phi_1 U/100,$$
 (2)

where

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 $T_{o} = \text{expired air temperature (}^{\circ}C)$

 ϕ_{i} = relative humidity of inspired air (percent)

 U_{o} - expired air temperature when $\phi_{i} = 0\%$ (°C)

 $U = U_S - U_O =$ the maximum difference in expired air temperatures associated with humidity of inspired air $\binom{O}{C}$

 $U_{s} = \text{expired air temperature when } ^{5}_{i} = 100\% (^{\circ}\text{C}).$

The lower curve is a linear function of $\mathbf{T}_{\mathbf{i}}$, the temperature of inspired air,

$$U_0 = 28 + 0.1 T_1$$
 (3)

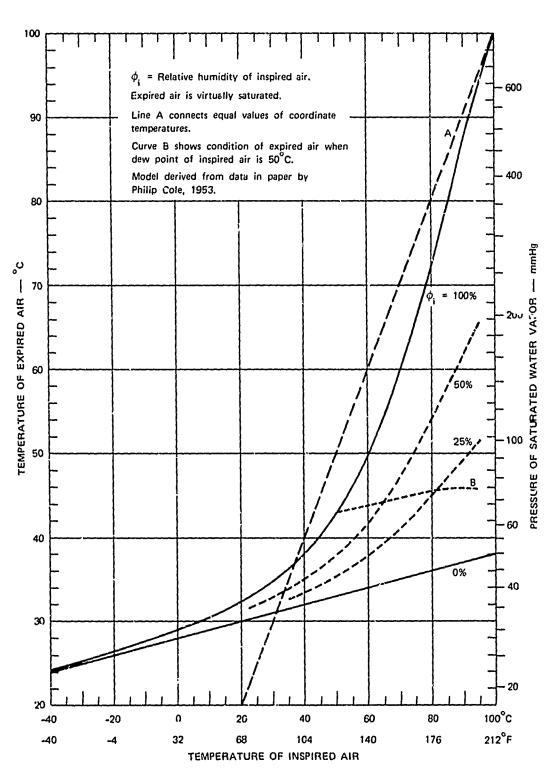


FIGURE 3 THERMAL PROPERTIES OF RESPIRED AIR

and the temperature difference, U, is an exponential function of $\mathbf{T}_{\mathbf{i}}$,

$$U = \exp(0.040819T_i + 0.0001325T_i^2 - 0.0000000128T_i^4)$$
 (4)

The numerical coefficients in Eq.(4) were determined by the following criteria:

- $T_e = 29^{\circ}C$ when $T_i = 0^{\circ}C$.
- $T_e = 37^{\circ}C$ when $T_i = 37^{\circ}C$.
- $T_e = 100^{\circ} C$ when $T_i = 100^{\circ} C$.
- $dT_e/dT_i = 1$ when $T_i = 100$ °C.

The first two criteria are salient data points that in themselves determine an exponential equation, $U=e^{0.045073T}$, which suggests that

$$T_e > T_i$$
 when $T_i > 87^{\circ}C$.

The third and fourth criteria merge the two temperatures at 100° C and avoid this apparent incongruity.

Values of respiratory parameters based on Eq. (2), (3), and (4) are shown in Table 1 for a pulmonary ventilation rate of one kilogram of inspired dry air per hour, which from Eq. (1) corresponds to a metabolic rate of about 167 ...logram calories per hour. Column 1 shows the relative humidity of inspired air, and Column 2 is the humidity ratio times 100. Each group of three relative humidities is identified with an inspired air temperature and a corresponding saturation pressure, PS. Column 3 is the humidity ratio of expired air times 100, and Column 4 is the temperature of expired air on the Celsius scale. Column 5 is the mass of moisture added to or extracted from the respired air in grams per hour. Column 6 is the latent heat of vaporization for moisture added or extracted, in kilogram calories per hour. Column 7 is the sensible heat associated with the temperature difference, T_e - T_i, in kilogram

TABLE 1
PROPERTIES OF RESPIRED AIR

	PROPERI	155 05	RESPIRED AIR		
INSPIRED AIR	EXPIRED	AIR	MOISTX LATENT	SENSEX	EXPRES
RH # W+100	W#100	SATEMP	GRM/HR KCL/HR	KCL/HR	MMH G
			. O . O.C. AC- OO . MMU.C.		
		+23.00	+2.9514E-02 MMHG +17.81 +10.34	+17-82	21.066
0 0.00000 50 0.00121		+23.08	+17.59 +10.38	+17.84	21.173
100 0.00243		+23-17	+17.97 +10.43	+17-87	21.280
INSPIRED AIR TEM			+9 . 6252E-02 MMHG	-	
0 0.00000		+24.00	+18.95 +10.99	+15-64	22.375
50 0.00396		+24.12	+19.05 +11.05	+15.67	22.533
100 0.00792		+24.23	+19-15 +11-11	+15.70	22.692
INSPIRED AIR TEM	P= -30 • 0		+2.8488E-1 MMHG		
0 0.0000	2.01605	+25.00	+20.16 +11.69	+13-46	23.755
50 0.01172	2.03648	+25 • 16	+20-25 +11-74	+13+50	23.988
100 0.02344	2.05709	+25.33	+20.34 +11.79	+13-54	24.223
		+26·00	+7.7387E-01 MMHG +21.44 +12.42	+11.27	25.209
0 0.00000	2 · 1 43 68 2 · 1 7 439	+26.23	+21.43 +12.41	+11-33	25.557
50 0.03183 100 0.06369		+26.47		+11-39	25.911
100 0.06369			+1.9480E+00 MMHG		
0 0.00000	2.27862	+27.00	+22.79 +13.20	÷9.07	26.739
50 0.08016	2.32579	+27.34		+5 - 17	27.272
100 0 1 6 0 5 3	2 - 37384	+27 - 67		49.26	27.815
INSPIRED AIR TEM	P= +0.0	C. PS=	+4.5813E+00 MMHG		
0 0.00000	2 - 42126	+28.00	+24.21 +14.02	+6-87	28 • 349
50 0-18882	2 • 49 5 6 0	+28 - 50	+23.07 +13.35	+7.01	29 • 186
100 0.37879	2.57202	+29.00	+21.93 +12.69	+7-15	30 • 0 44
			+9.2049E+00 MMHG		20.044
0 0.00000	2 • 57202	+29.00	+25.72 +14.88	+4•67 +4•88	30 • 0 4 4 31 • 39 3
50 0.38058	2 • 69259	+29.76	+23.12 +13.37 +20.52 +11.87	+5.09	32 • 795
100 0.76585	2.81835	+30 - 52	+1.7531E+01 MMHG	+3+07	324 173
	2.73131	+30.00	+27.31 +15.80	+2.46	31.826
0 0.00000 50 0.72895	2.93270	+31-17	+22.04 +12.74	+2 - 78	34.066
100 1 • 47 519	3.14767	+32-38	+16.72 +9.66	+3-10	36 - 441
IN SPIRED AIR TEN	1P= +30 • 0		+3.1826E+01 MMHG		
0 0.00000	2 - 899 61	+31.00	+29.00 +16.76	+0.25	33 • 699
50 1 • 33631	3 • 2 4 5 3 9	+32.90	+19.09 +11.03	+0 • 72	37.516
100 2.73131	3 • 62895	+34.79	+8.98 +5.18	+1.22	41 • 703
IN SPIRED AIR TEN			+4.7076E+01 MMHG		25 244
0 0.00000	3.02304	+31 - 70		-1.31	35.066
50 1.99761	3 • 53557	+34.35		-0.67	40 • 658
100 4.12780	4.12780	+37.00	+0+00 +0+00	÷0•00	47.076
*********	40.0	C. DC=	AS. STOREAGE MANG		
	3.07740	+32.00	+5.5338E+01 MMHG +30.77 +17.78	-1.98	35 • 666
0 0.00000 50 2.36176	3.68623	+35.06	+13.24 +7.64	-1-25	42.324
100 4.90995	4.40563	+38 - 12	-5.04 -2.91	-0 - 49	50 • 033
INSPIRED AIR TE		C. PS=	49.2554E+01 MMHG		
0 0.00000	3-26519	+33.00	+32.65 +15.86	-4.20	37.733
50 4.05564	4 • 361 35	+37.95	+3.06 +1.76	-3-12	49.564
100 8 67709	5.79688	+42.90	-28.80 -16.55	-1.93	64.474
INSPIRED AIR TE	4P≖ +60•0		+1 - 49 46E+ 32 MMHG		
0 0.00000	3.46354	+34.00	+34.64 +19.99	-6.44	39.904
50 6.82673	5 • 47634	+41.90		-4.83	61 • 200
100 15:33683	2-58126	+49.80		-2.98	91.657
INSPIRED AIR TE			+2.3379E+02 MMHG	-8 - 69	42 • 151
0 0.00000	3 • 67300	+35.00		-6.39	80-669
50 11.38460	7 • 42856	+47.26	-39.56 -22.69 -129.58 -73.86	-3.49	146-129
100 27.87069	14.91301 MP: +80.0		+3.5528E+02 MMHG	3. 7/	
O 0.00000	3.89420	+36.00		-10.94	44.570
50 19:10717	10-94783	+54-10		-7.90	113-123
100 55-15957	32 • 06338	+72.21	-230.96 -130.81	-3.34	257-014

calories per hour. Column 8 is the vapor pressure of saturated water vapor in expired air in millimeters of mercury. The values in Columns 5, 6 and 7 may be either positive or negative, and should be multiplied by 0.60 for a metabolic rate of 100 kcal/hr.

The range of inspired air temperatures in Figure 3 extends upward to 100°C (212°F). If the relative humidity is very low, air at this high temperature can be breathed without pain or injury; in fact, whole body exposure in such an environment can be tolerated for a short time, as in a sauna bath. 47,48 In saturated air, tolerance time for whole body exposure would be short at 40° C (104° F), and at dew point temperatures on the order of 50°C (122°F), condensation of hot water on the skin or nasul mucosa may be painful. Lind found that respiratory discomfort was first apparent in saturated air at 39°C (102°F) in connection with mine rescue operations. Killick (quoted by Lind) had noted incipient discomfort at 54.5°C (130°F) for men at rest and 51.5°C (125°F) for men at work. Haldane noted that respiration in saturated air at 54.5°C (130°F) was slightly painful, at 48.9° C (120°F) work has hardly possible, and at 45°C (113°F) breathing was not difficult. On Figure 3, curve B (dashed line) is the locus of points having a dew point of 50° C (122 $^{\circ}$ F). Therefore, curve B is essentially an upper limit for transient exposure during a fire in a hot confined environment. On Figure 3, the curve for ϕ_i = 100 percent at inspired vir temperatures higher than 50°C is needed for interpolation when the relative humidity of inspired air is less than 100 percent.

Diffusion of Moisture Through Dry Skin

A simple diffusion concept for the insensible loss of moisture through dry skin can be defined in terms of latent heat loss by the relationship,

$$H_{d} = K_{d}A_{d}(P_{S} - P_{V}), \qquad (5)$$

where

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H_d = metabolic heat dissipated in vaporization of diffusing moisture
 (kcal/hour)

 $A_d = \text{area of dry skin } (m^2)$

 P_c = saturation pressure at skin temperature (mmHg)

P = partial pressure of water vapor in air (mmHg)

K_d = diffusion constant [kcal/(hr.m².mmHg)]

to obtain experimental data in which this relatively small effect is not obscured, sweat gland activity must be suppressed. This has been accomplished in several sets of experiments planned for the purpose by

 Performing tests at environmental temperatures in which active sweating does not occur⁵⁰⁻⁵²

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- Using drugs (such as atropine) that inhibit sweating. 53,54
- Selecting subjects who do not have sweat glands.

When environmental temperatures are within the range of 21°C to 28°C, with skin temperatures less than 34°C, the values of K_d in Eq. (5) are characteristically within the range of 0.2 to 0.5 [kcal/(hr.m².mmHg)].50-53 In general, the indicated values of K_d tend to increase with air or skin temperature, but higher values obtained at air temperatures above 29°C or skin temperatures above 34°C may reflect the effects of sweat gland activity.51-53 The works of some investigators suggest a more complex relationship than that defined by Eq. (5).53,56,57

For the purposes of this study, a value of $0.35 \, [\, kca1/(hr.m^2.mmlig)]$ is used for the diffusion constant, K_d , in Eq. (5). This is consistent

with the value used in some recent studies of human comfort. 12,14 The diffusion of moisture through skin surfaces is essentially a mass transfer process that can be halted by an impervious covering. It is also quite apparent that the process can be attenuated by layers of clothing in proportion to the effective permeability of the skin clothing system. 13,14 Some of the computations in the present study of metabolic parameters include an attenuation factor, F_e , the magnitude of which is inversely proportional to the insulating value of clothing,

$$F_{e} = \frac{1}{1 + 0.1 \text{ K}}$$
 (6)

where K is the thermal resistance of clothing in "clo" units. A clothing ensemble that has a resistance of L clo would have a surface-to-surface temperature difference of 0.18° C when conductive heat flux is 1 kcal/(hr.m²).

Evaporation of Sweat

The production and evaporation of sweat is a metabolic process that is used under physiological control for maintaining thermal equilibrium in a warm environment. When evaporative cooling is needed, the control mechanism adjusts the wetted area of skin surfaces in accordance with the requirement. The series of environmental conditions, this cooling effect attains a maximum value when skin surfaces become completely wet or when the maximum rate of sweat production is reached. The maximum sustained rate of sweat product. for a "standard" man is about one liter per hour, and the potential soling effect of this fluid is about 600 kcal/hr or 2400 Btu/hr. Metabolic requirements for lesser rates of evaporative cooling may be limited by upor pressure differentials or relative velocities of air motion in the environment. The effect is defined by the equation

$$E_{\text{max}} = h A (P - P)$$
 (7)

where

E metabolic heat dissipated by evaporation of sweat when skin surfaces are completely wet.

 A_{o} = effective area of skin surface (m²)

 P_{s} = saturation pressure at skin temperature (mmHG)

P = partial pressure of water vapor in air (mmHg)

h_e = evaporative heat transfer coefficient [kcal/hr.m².mmHg)].

The evaporative heat transfer coefficient, h_e , and the convective heat transfer coefficient, h_c , are both sensitive to air velocity and can be correlated through the Lewis relation. In connection with metabolic heat/mass transfer

$$h_{e} \approx 2h_{c} \tag{8}$$

when the coefficients are expressed in units of $[kcal/(hr.m^2.mmHg)]$ and $[kcal/(hr.m^2.^{\circ}C)]$. This relationship has been demonstrated by Woodcock⁶² and Brebner, Kerslake, and Waddell.⁶³,⁶⁴

Convective Heat Exchange

The transfer of metabolic heat by convection can be determined by the equation.

$$H_{c} = h_{c} A_{c} (T_{c} - T_{a})$$
(9)

where

 $H_c = \text{heat transfer at exposed surfaces of skin or clothing (kcal/hr)}$

 $A_c = \text{effective area of exposed skin or clothing surfaces (m}^2$)

 $T_c = mean temperature of exposed surfaces (<math>^{\circ}C$)

 $T_a = temperature of environmental air (<math>^{\circ}C$)

h = convection heat transfer coefficient [kcal/hr.m².°c)]

The convective heat transfer coefficient, h, is sensitive to variations in relative air velocity. For numerical computations in connection with this study, a basic value of $h_c = 4.0$ is assumed to be representative for sedentary persons in shelters. According to Fanger 11 and Winslow, Gagge, and Herrington, 65 this value is appropriate for a relative air velocity of about 15 cm/s or 30 ft/min. For purposes of comparison. other computations are made in which h_c is assigned values of 3.4, 5.0, and 7.0 kcal/(hr.m².°C). These supplementary values are associated respectively with relative air velocities of about 11, 23, and 45 $\,\mathrm{cm/s}$ or 21, 45 and 90 ft/min. The value of $h_c = 3.4 \text{ kcal/(hr.m}^2.\text{°C})$ or $h_c = 3.4 \text{ kcal/(hr.m}^2.\text{°C})$ 0.7 Btu/(hr.ft². F) is the minimum value obtained with very low velocities of ventilating air in a monoman calorimeter in which radiant heat transfer is suppressed by a reflective interior surface. Spontaneous movements by the sedendary test subjects created sufficient relative motion to prevent the occurrence of lower values for the convection coefficient. The effective surface area for conductive heat transfer is

$$A_{C} = F_{C} A_{S}, \qquad (10)$$

where

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 A_s = effective area of skin surface, i.e., the total skin surface excluding areas insulated by chair seats or backs (m^2)

 F_c = the ratio of exposed surface areas for clothed and nude persons. In this study the value of F_c is determined by the equation 11,12

$$F_c = 1 + 0.1 K_c$$
 (11)

where K_{c} is the insulating value of clothing in clo units.

Radiative Heat Exchange

In this study the transfer of metabolic heat from skin or clothing surfaces to the environment is determined in accordance with the Stefan-Boltzmann law in preference to a linear approximation.⁶⁶,⁶⁷ This permits a more realistic comparison of relative effects over a wide range of temperatures. The fundamental equation is

$$H_{r} = A_{r} K_{r} (T_{r}^{4} - T_{w}^{4})$$
 (12)

where

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H = heat transfer by radiation to or from exposed surfaces of skin
 or clothing (kcal/hr)

 $A_r = \text{effective area of exposed skin or clothing surfaces (m}^2$)

T = mean <u>absolute</u> temperature of exposed skin or clothing surfaces

(OK)

 T_{W} = mean radiant temperature of walls, furnishings and other surfaces "seen" by the subject, including other people (O K)

 K_r = the product of thermal emissivity of exposed skin and clothing surfaces (ϵ) and the Stefan-Boltzmann constant (σ).

The effective area, A_r , of skin and clothing surfaces for heat transfer by radiation is influenced by posture and is appreciably less than the aggregate area of skin or clothing surfaces.^{67,68} Thus,

$$A_{r} = F_{r}A_{c} \tag{13}$$

where A_c is defined by Eq. (10) and F_r is a dimensionless correction factor. In the present study, computations relating to the transfer of metabolic heat by radiation will be based on the values, $F_r = 0.65$, which is appropriate for an individual in a seated position, $^{11},^{67},^{68}$ and $K_r = 4.8 \times 10^{-8} \text{ kcal/(hr.m}^2.\text{c}^4)$, which implies an effective emissivity of about 98 percent. $^{11},^{24}$ To simulate the effects of a densely populated space, computations will include several values for T_w , the mean radiant temperature of the environment (0 K), 2s follows:

- $T_{W} = T_{a} + 273$
- $T_{w} = T_{s} + 273$
- $T_{W} = (T_{S} + T_{a})/2 + 273$

where T_a and T_s are the air and mean skin temperatures (${}^{\circ}$ C), respectively.

Heat Conduction Through Clothing

The sensible heat conducted through clothing corresponds to that transferred to the environment by convection and radiation at exposed surfaces. The fundamental equation is

$$H_0 = A_0 (T_s - T_0) / (0.18 K_c)$$

where

H = heat flux through clothing (kcal/hour)

 A_0 = skin surface area excluding parts insulated by contact with furnishing (m^2)

 $T_{s} = \text{mean skin temperature } (^{\circ}C)$

 $T_{O} = mean temperature of exposed clothing surfaces (<math>^{\circ}C$)

 $K_c =$ thermal resistance of clothing (clo units).

In this study, the thermal resistance of clothing, $K_{\rm c}$, is an independent variable used to maintain thermal equilibrium at environmental temperatures below the threshold for sweating or evaporative regulation. Evaporative regulation is reserved for persons who are virtually nude.

Simultaneous Effects

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The results of this study of relationships among metabolic parameters were obtained with a computer program ir which the effects of the component processes for heat transfer are combined to interact and to proceed simultaneously. The program was synthesized under the following criteria:

- People in the shelter space are engaged in sedentary activities
 and are in thermal equilibrium with the prevailing environment.
- When environmental conditions of temperature and humidity are above the threshold at which the evaporation of sweat becomes necessary for maintaining thermal equilibrium, the people are virtually nude. Below this threshold, thermal equilibrium is maintained by adding increments of clothing, as necessary. Below this threshold, transfer of metabolic moisture is associated with the mechanisms of respiration and diffusion through dry skin, but not with sweat gland activity.
- At any air temperature, T_a C, the mean skin temperature, T_s C, is defined by the equation

$$T_s = 34 + 1.5 \arctan[0.1967(T_a - 31)].$$
 (15)

Skin temperatures determined with Eq. (15) are shown by the curve at the top of Figure 4. Several skin temperatures are 89.6°F, 91.4°F, 93.2°F, 95.0°F and 96.8°F when air temperatures are, respectively, 50.0°F, 80.6°F, 87.8°F, 95.0°F and 125.6°F.

The objective in using a curve of the shape defined by Eq. (15) is to simulate a well-defined transition between the zone of cool environments, in which thermal equilibrium is maintained by variations in clothing insulation, and the zone of warm environments, in which thermal equilibrium is maintained by production and evaporation of sweat.

• At any environmental state there are two rates of latent heat transfer that are associated with active sweating. One, E req, is the rate of evaporative cooling required to maintain thermal equilibrium. The other, E max, is the maximum rate of evaporative cooling that can be attained in the environment when the skin is completely wet, as defined by Eq. (7). The skin wetness is here defined as the ratio,

$$R_{W} = \frac{E_{req}}{E_{max}}$$
 (16)

where the quantities E_{req} and E_{max} include the evaporation of sweat, but do not include vapor diffused through dry skin nor moisture transferred in the respiratory tract. However, moisture continues to diffuse through any dry portion of skin surface in accordance with Eq. (5). Heat storage and a consequent rise in body temperature would occur only when $E_{req} = E_{max}$, and the rate of heat storage is then

$$S = E_{\text{max}} - E_{\text{req}} \text{ kcal/hr}$$
 (17)

The condition, $E_{req} = E_{max}$ determines a limiting environmental state for which the "relative strain index" is unity.

Graphic Comparison of Metabolic Data

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Computations needed for the graphic comparison of data relating to each of the contributing processes for metabolic heat transfer are based on the following set of physical and physiological parameters:

Barometric pressure = 1.0 atmosphere

Body temperature = $37^{\circ}C$

Metabolic rate, M = 100 kcal/hr

External work = 0

Skin surface (DuBois correlation) = 2.0 m^2

Effective skin surface, $A_{s} = 1.9 \text{ m}^2$

Radiation area of nude skin, $A_r = 1.3 \text{ m}^2$

Radiation coefficient, $K_r = 4.8 \times 10^{-8}$ (invariant)

Convection coefficient, $h_c = 4.0 \text{ kcsl/(hr.m}^2.^{\circ}C)$

Evaporation coefficient, $h_e = 8.0 \text{ kcal/(hr.m}^2.\text{mmHg)}$

Pulmonary ventilation, G = 0.60 kg of dry air inspired per hour.

Results of the computations are presented in Figures 4 through 6. All computed data are shown as functions of air and wall temperature over the range of 0° C to 80° C. All data that are plotted as solid or dashed lines or curves are based on values of moisture diffusion through dry skin that are not atter—ed by clothing. In addition, each figure shows two or more rows of prominent dots that indicate the effect of attenuating this diffusion process by the factor, $F_{\rm e}$, as defined by Eq. (6). There is no attenuating effect when the thermal resistance of clothing is 0 clo units.

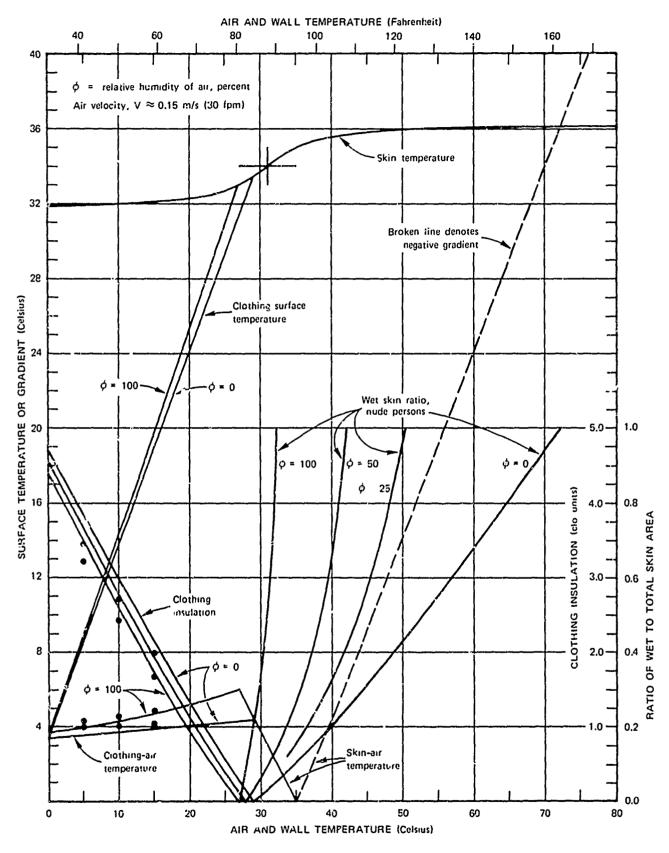
Skin and clothing temperatures, surface-to-air temperature differences, required insulating values for clothing, and ratios of wet to total skin areas are shown in Figure 4. In the cool zone, the temperature gradient from exposed clothing surfaces to the surrounding air is relatively small and does not change very much with air temperature. The effects of extreme changes in relative humidity are not very important. The thermal resistance of clothing required at 10°C (50°F), the minimum temperature for a shelter environment, is about 3 clo units.

In the warm zone, skin-to-air temperature differences increase rapidly with temperature but are unaffected by changes in relative humidity. However, the ratio of wet to total kin surface is very sensitive to changes in relative humidity. When this ratio becomes 1.0, no further increase in the rate of evaporative cooling is possible.

The sensible/total and latent/total metabolic heat ratios are evaluated in Figure 5. The effect of changes in relative humidity on the heat ratios at air temperatures of about 25° is significant. The postulated effect of clothing on the diffusion of vapor through dry skin is also significant. This attenuating effect is indicated by the rows of dots in the lower left corner. These dots relate to the adjacent curves for 0 to 100 percent relative humidity.

In connection with warm environments, the broken lines determine values for the latent/total metabolic heat ratio when the required rate of evaporative cooling is greater than the maximum attainable (that is, thermal equilibrium is not possible and an increase in body temperature is inevitable). The broken lines and the solid lines intersect at state points where $E_{\text{reg}} = E_{\text{max}}$ and skin surfaces are completely wet.

Contributions made by six heat transfer processes to maintenance of thermal equilibrium are evaluated in Figure 6 for three values of relative humidity--0, 50 and 100 percent. Heat transfer rates are expressed on



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FIGURE 4 CHARACTERISTIC TEMPERATURES AND RELATED METABOLIC PARAMETERS FOR SEDENTARY PERSONS IN THERMAL EQUILIBRIUM

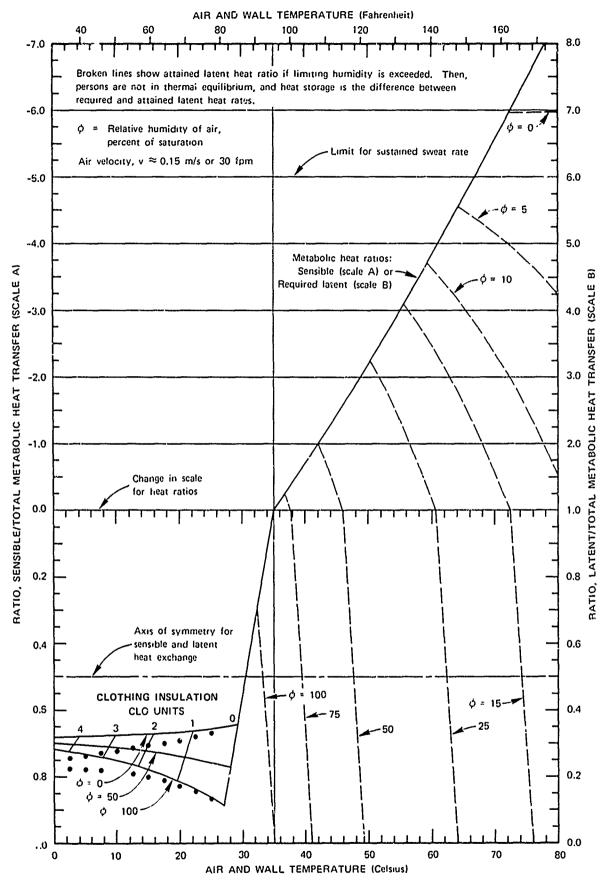
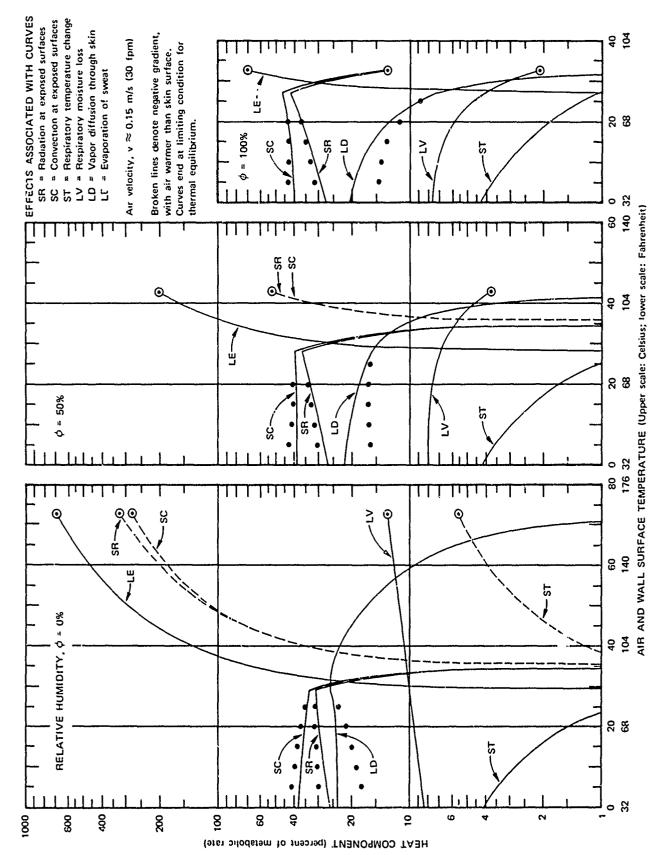


FIGURE 5 TRANSFER OF METABOLIC HEAT TO A TYPICAL ENVIRONMENT FROM SEDENTARY PERSONS IN OPTIMUM CLOTHING



COMPONENTS OF METABOLIC HEAT ASSOCIATED WITH THERMAL EQUILIBRIUM FOR SEDENTARY PERSONS IN OPTIMUM CLOTHING FIGURE 6

a logarithmic scale 1 percentages of metabolic rate as functions of air and wall temperatures. Each curve is identified by a symbol in accordance with explanatory notes. The curves terminate near the right side of each part of the figure at a state point for which $E_{req} = F_{max}$. This point is identified by an encircled dot. Radiative effects are less than convective effects in a cool environment, but are more than convective effects in a warm environment. For environments in which thermal equilibrium is maintained by optimum use of clothing, effects of this clothing in attenuating vapor diffusion through dry skin are indicated by rows of dots as in Figures 4 and 5.

Tables of numerical data relating to transfer of metabolic heat and moisture, the associated program listing, and explanatory notes are contained in Appendix A.

III SHELTER VENTILATION

Ventilation Process Lines

The metabolic data shown in Figure 5 suggest that the ratio of latent to total metabolic heat transfer can be adequately represented throughout the range of environmental conditions in which thermal equilibrium can be maintained by a constant and a linear equation,

$$0 = 0.25 \tag{18}$$

when $T \leq 82.5^{\circ}F$, and

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$$0 = 0.06T - 4.7 \tag{19}$$

when $T \ge 82.5^{\circ}F$. In these expressions, $\mathfrak o$ is dimensionless ratio of latent to total metabolic heat transfer and T is the environmental air temperature (Fahrenheit). In conjunction with equations for the thermodynamic properties of moist air and the following assumptions, these relationships determine equations for families of ventilation process lines:

- Ventilating air moves linearly through the occupied space,
 from one wall to an opposite wall.
- Metabolic heat and moisture are added gradually to air passing through the occupied space.
- There are no sources of heat or moisture other than metabolic effects. This implies that lighting loads and heat transmitted through walls and roof are relatively small and negligible.

When air temperatures are less than or equal to 82.5°F, equations for the family of ventilation process lines associated with Eq. (18) can be expressed as a function of specific enthalpy, H, and humidity ratio, W,

$$H - H_{O} = 4222 (W - W_{O}) \tag{20}$$

or as a function of humidity ratio, W, and air temperature, T,

$$\frac{0.5508 + W}{0.5508 + W_O} = \frac{7246 - T_O}{7246 - T} \tag{21}$$

When air temperatures are greater than or equal to 82.5° F, an equation for the family of process lines associated with Eq. (19) is

$$\frac{0.5508 + W}{0.5508 + W_{O}} = R_{2} \left(\frac{R_{3}}{R_{2}}\right)^{0.006944}, \tag{22}$$

where

$$R_2 = \frac{2305 + T_0}{2305 + T}$$

$$R_{3} = \frac{95 - T_{0}}{95 - T} .$$

In Eqs. (20), (21), and (22), $T_{\rm O}$, $W_{\rm O}$, and $H_{\rm O}$ are properties of moist air at any state point on a particular ventilation process line, and T, W, and H are properties of moist air at any other point on the same process line. Equations (20) and (21) are not valid when air temperatures are higher than $82.5^{\circ}\mathrm{F}$, and Eq. (22) is not valid for temperatures lower than $82.5^{\circ}\mathrm{F}$. The equations are not valid when the air is supersaturated. The units in these equations are

• Temperature, T (OF)

- Humidity ratio, $W = \frac{\text{pounds of moisture}}{\text{pounds of dry air}}$
- Specific enthalpy, H = Btu/lb of dry air.

Equations (20), (21), and (22) determine the locus of state points (on a psychometric chart) that develop in sequence as a stream of ventilating air moves through an occupied space.

This study is particularly concerned with ventilating systems that conserve heat for tempering purposes by partial recirculation of air during cold weather. In such a system there are three salient points of interest:

- (1) The state of fresh air
- (2) The state of mixed air supplied to the space
- (3) The state of air that is either recirculated or exhausted to atmosphere.

To identify air properties associated with each of these points, the corresponding item numbers above are used as subscripts. Then, if a space is occupied by sedentary persons in thermal equilibrium with a metabolic rate of M=400 Btu/hour/person, the rate of air supply to the space must be

$$V_{2} = \frac{400}{4.5 (H_{3} - H_{2})}$$

$$= 88.89 / (H_{3} - H_{2})$$
(23)

where

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Y, = rate of ventilation (SCFM per person)

H₃ = specific enthalpy of air leaving the space (Btu/lb of dry air) H_2 = specific enthalpy of air entering the space (Btu/lb of dry air).

The associated flow rate of fresh (outside) air is

$$v_1 = 88.89 / (H_3 - H_1),$$
 (24)

where

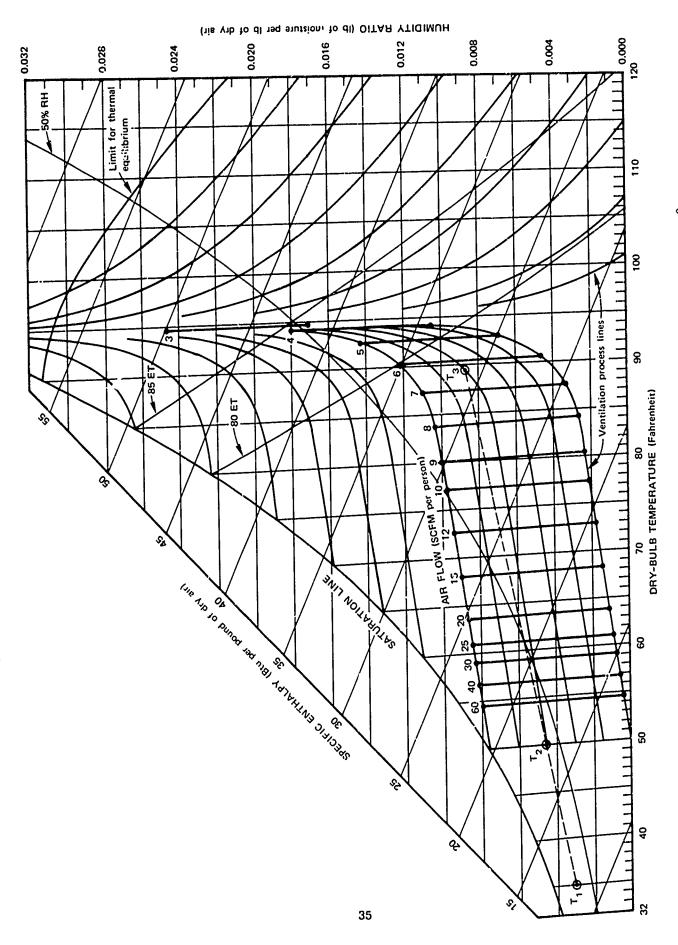
v₁ = flow rate of fresh air (SCFM/person)

H₁ = specific enthalpy of fresh air (Btu/lb of dry air).

Several ventilation process lines determined analytically by Eqs. (20), (21), and (22) are shown on Figure 7. These lines resemble process lines based on experiments performed by Pefley, Cull, and Sekins. The six lines that originate at a temperature of $50^{\circ}F$ bracket the possible range of 0 to 100 percent relative humidity. Thus, these lines represent process lines associated with the prescribed criterion for a minimum temperature of $50^{\circ}F$ in a shelter environment. Across this group of six process lines are a number of heavier lines that terminate at dots. These are isoventilation lines, based on Eq. (23), with the proviso that air is supplied to the shelter space at a temperature of $50^{\circ}F$. Each isoventilation line is labeled with the associated ventilating rate. A curve at the top of the chart shows the locus of points above which thermal equilibrium cannot be maintained. This line was determined from data in Figures 4 and 5 at state points where $E_{\text{req}} = E_{\text{max}}$. Effective temperature lines for 80 ET and 85 ET are also shown.

Seasonal Recirculation of Air

If a shelter ventilating system of either the supply or exhaust type is so arranged that fresh air enters an occupied space through a few openings with little or no distribution, environmental temperatures in



PROCESS LINES FOR VENTILATING A SPACE WITH MIXFD AIR AT 50°F FIGURE 7

the vicinity of these openings will not differ greatly from the outside temperature. During cold weather, temperatures may frequently be less than 50°F over a large part of the shelter space. This stressful condition could be eliminated by tempering or heating the fresh air. If heating apparatus is not provided (or is inoperable), the cold areas can be reduced or eliminated by recirculating part of the ventilating air. Partial recirculation is often used in air conditioning practice to reduce heating or cooling loads.

On Figure 7, the dashed line connecting three encircled dots at $T_1 = 35^{0}\mathrm{F}$, $T_2 = 50^{0}\mathrm{F}$, and $T_3 \approx 89^{0}\mathrm{F}$ illustrates the geometrical configuration associated with a recirculating system for ventilating an occupied space. The dashed line is straight because the oblique coordinates on this psychrometric chart are specific enthalphy, H, and humidity ratio, W: the lines of constant temperature are not parallel. Basic properties of moist air at the three state points are T_1 , W_1 , and W_1 for the fresh air; W_2 , and W_2 for the mixed air; and W_3 , and W_3 for the recirculated air. Points 2 and 3 must be on the same ventilation process line. In accordance with the principle of conservation of mass and energy in a mixing process, the properties of moist air at the three state points are related by the equations,

$$\frac{H_3 - H_1}{W_3 - W_1} = \frac{H_2 - H_1}{W_2 - W_1} = \frac{H_3 - H_2}{W_3 - W_2}$$
 (25)

and the ratio of flow rates for fresh and mixed air is

$$\frac{V_1}{V_2} = \frac{H_3 - H_2}{H_3 + H_1} = \frac{W_3 - W_2}{W_3 - W_1} . \tag{26}$$

Equations (18) through (26), together with precise relationships among psychrometric quantities (saturation pressure, humidity ratio, specific enthalpy, and temperature), were used as the basis for an iterative

computer program that determines the required flow rate for fresh air and evaluates properties of moist air at state points for fresh, mixed, and recirculated air when the input parameters are as follows:

- Flow rate of mixed air, V_2 (SCFM/person). This corresponds to the rated unit capacity of the ventilating system.
- Temperature of mixed air, T_2 (OF).
- Temperature of fresh air, T_{I} (OF).
- Relative humidity of fresh air, ϕ_1 (%).

The program rejects combinations of input data that would lead to recirculated air having a dew point in excess of 90°F, which is just above the limit for metabolic equilibrium, or to supersaturated mixed air. If these causes for rejection occur, the program determines the minimum ventilating capacity that would satisfy these requirements.

Figure 8 is constructed with data calculated using the above program. This chart evaluates parameters associated with a recirculating system for ventilating a shelter with mixed air at a temperature $T_2 = 50^{\circ} F$, when the fresh air temperature, T_1 , is less than or equal to $50^{\circ} F$. Since the prescribed minimum temperature for a shelter environment is $50^{\circ} F$, Figure 8 determines limiting parameters for design or operation of such systems. For example: If the unit capacity of a ventilating system is 12 SCFM per person, and the outside air temperature is $20^{\circ} F$, the temperature of recirculated air will be $72.6^{\circ} F$, the flow rate of fresh air should be 5.2 SCFM per person, and the humidity ratio of air leaving the shelter space will be higher than the humidity ratio of fresh air by about 0.004 pounds of moisture per pound of dry air.

On Figure 8, the blank area labeled "Fog" denotes conditions under which the mixed air would be supersaturated, if the fresh air were dry.

The boundaries of this fog region if the fresh air were saturated are indicated by two short dashed curves. The lower dashed curve and the adjacent solid line indicate ventilating rates below which the dew point of recirculated air would be more than 90°F and an increase in body temperatures should be expected.

Tables of numerical data relating to partial recirculation of ventilating air, the associated program listing, and explanatory notes are contained in Appendix B.

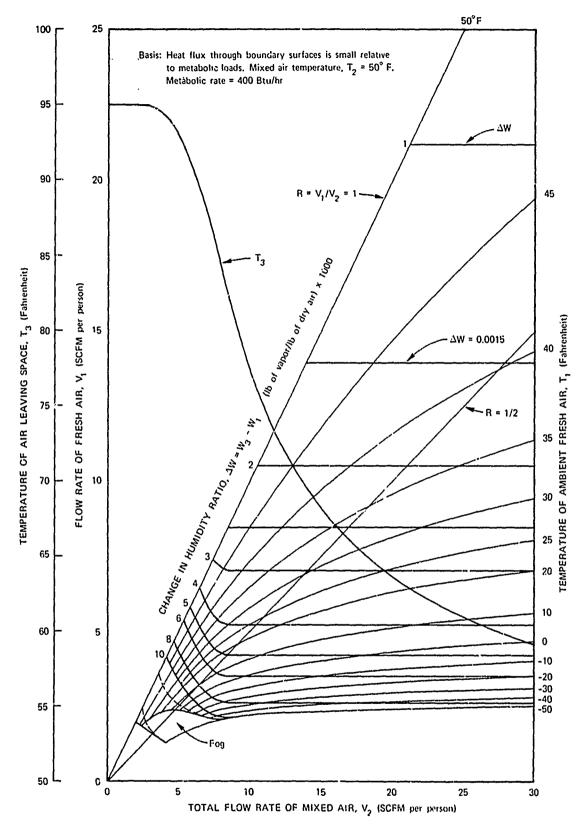


FIGURE 8 VENTILATION OF AN OCCUPIED SPACE WITH MIXED FRESH AND RECIRCULATED AIR AT 50°F

IV CONCLUSIONS AND RECOMMENDATIONS

Conclusions

Among elements that collectively determine the condition and variabilities of the environment in a ventilated shelter are several major factors:

- Prevailing ambient conditions with respect to air temperature and humidity.
- Size, shape, and compartmentation of the space, and furnishings provided therein.
- Utilization of the space with respect to number of people and duration of occupancy.
- Metabolic responses of each person to his local macroclimate with regard to physical activity and transfer of heat and moisture.
- Lighting and other internal heat sources supplementary to metabolic effects.
- Thermal characteristics of the structure with respect to transient and steady-state heat transfer.
- · Per capita and total capacities of the ventilating system.
- · Configuration of the ventilating system.

If a shelter were densely populated, the transfer of metabolic heat and moisture would be modified by the proximity of one person to another. The mean radiant temperature at any point in the shelter would be determined by temperatures of skin or clothing surfaces as well as temperatures

of wall and ceiling surfaces. Also, the flow of air through the space would be diverted by obstructions (people) near the floor to clear channels near the ceiling. The effect of this diversion would be to stratify the environment. Air velocities in the living space near floor level would be lower than air velocities in the overhead space. Consequently, capabilities for heat transfer by convection and evaporation of sweat would be reduced in the living space by an increase in population density. The establishment of vertical convection currents would be necessary to transfer of heat and moisture from lower to upper levels. Thus, temperatures and humidities in the living space would be somewhat higher than in the air stream overhead. The effects of population density on comfort in a shelter environment may be either adverse or beneficial, as determined by the season of the year and by relationships between metabolic parameters.

Section II, Metabolic Parameters, examines in some detail six biophysical processes for transfer of heat and moisture from the human body to its environment, first as isolated mechanisms, and then as simultaneous processes. A salient result of this study is a set of three figures (Figures 4, 5, and 6) that provide relatively complete information regarding metabolic responses in shelters occupied by sedentary persons dressed in optimum clothing. These data are based on an air velocity of about 30 feet per minute and equality of air and wall temperatures. Computations were also made with relative air velocities of about 20, 45, and 90 feet per minute, and with wall temperatures that are not equal to air temperatures. These supplementary data are included in nine numerical tables in Appendix A. It is possible to draw some tentative conclusions from these figures and tables, as follows:

- Data in Figure 6 show that proportional effects of the six processes for metabolic heat transfer are extremely variable at temperatures higher than about 30°C (86°F), but are comparatively stable at lower temperatures. Rates of heat transfer by radiation and convection do not differ greatly.
- Data in Figure 5 show that variations in humidity have a significant effect on the partition of metabolic heat losses into sensible and latent fractions at air temperatures of about 15°C to 27°C (60°F to 80°F). At higher temperatures, humidity has virtually no effect on the sensible/total or latent/total metabolic heat ratios, but has a sharply defined effect in determining limiting conditions for thermal equilibrium.
- Data in Figure 4 show that humidity has a strong effect on the ratio of wet to total skin areas in warm or hot environments.
- Data in Figure 4 also show that differences in temperature between clothing surfaces and air remain within the range of about 3°C to 6°C (4°F to 10°F). At a temperature of 30°C (86°F), the mean skin temperature is about 4°C (7°F) higher than air temperature. At a temperature of 40°C (104°F), the mean skin temperature is about 5°C (9°F) lower than air temperature. In a hotter environment, the air temperature increases at a much higher rate than skin temperatures because the skin is cooled by evaporation. These observations suggest that population density will not have a great effect on radiant heat transfer in the critical comfort range of 30°C (86°F) to 40°C (104°F). The effect of an increase in population density may be beneficial to thermal comfort in colder and hotter environments.

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Numerical data in Tables A-4, A-5, A-6, and A-7 of Appendix A are based on parameters that differ only with respect to relative air velocity and the associated values of coefficients for convection and evaporation, as shown in Table A-1. Numerical data in Tables A-4, A-8, and A-9 are based on parameters that differ only with respect to mean radiant temperature, as defined in Table A-1. A comparison among data from these tables indicates that the effects of an increase in population density on both relative air velocity and mean radiant temperature tend to lower the air temperature at which thermal equilibrium can be maintained without clothing and without evaporation of sweat. At any lower temperature, the amount of clothing required to maintain thermal equilibrium is also reduced by occupancy effects on either relative air velocity or mean radiant temperature. However, population density appears to have no significant effect on the ratio of latent to total heat transfer from clothed persons. In higher temperature ranges, which are characterized by active sweating and virtual nudity, increased occupancy tends to increase evaporative cooling requirements at air temperatures below 35°C (95°F), and to decrease these requirements at higher temperatures. The effects of changes in relative air velocity and mean radiant temperature on the latent/total heat ratio are shown graphically on Figure 9, which was constructed with data from Tables A-4, A-7, and A-8 in Appendix A. This figure also shows the effects of air velocity and radiant temperature on the limits for thermal equilibrium at two relative humidities, 50 and 100 percent. In Table A-8, mean radiant temperatures are equal to the temperatures of exposed skin or clothing, which implies complete suppression of radiative heat transfer. In Table A-5, heat/ mass transfer coefficients are appropriate with a relative air velocity of about 20 feet/minute, which tends to be minimal for sedentary

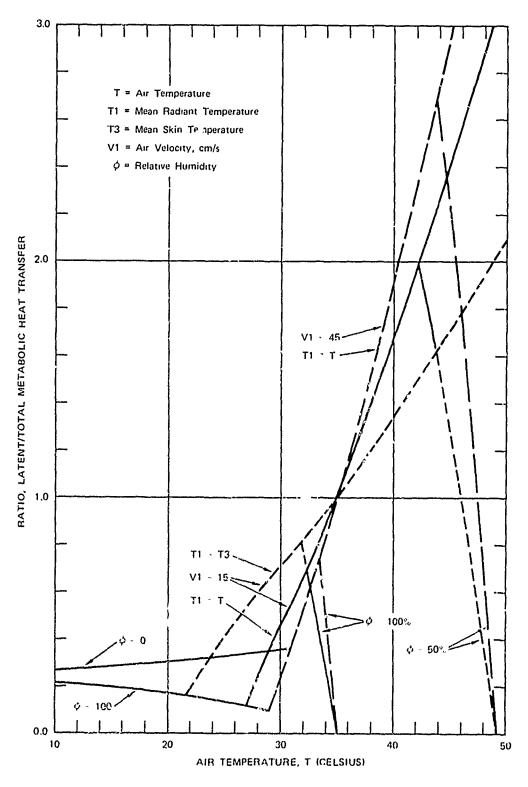


FIGURE 9 EFFECTS OF AIR VELOCITY AND MEAN RADIANT TEMPERATURE ON METABOLIC HEAT TRANSFER

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levels of physical activity. The metabolic data in Table A-9, which is based on a relative air velocity of about 30 feet per minute and a mean radiant temperature equal to the mean of environmental air and exposed skin or clothing temperatures, may be most representative for conditions likely to develop in shelters that are fully occupied by sedentary persons.

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Section III, Shelter Ventilation, uses metabolic data developed in Section II (Figure 5) as the basis for a study of shelter ventilation, with special emphasis on systems that recirculate air in cold weather. The ventilation process lines on Figure 7 represent loci of conditions that would develop in sequence along the path of air moving through a shelter. For all of these lines, the direction of air movement is toward the line for 95°F dry-bulb temperature from either lower or higher initial temperatures. At a temperature of 95°F, only evaporative cooling is effective because air, wall, and skin temperatures are equal at that model temperature. If air is supplied to an occupied space at a temperature of 50°F, those process lines that originate along the 50°F temperature line show the band of environmental conditions that could develop along the air stream. The vertical bars across this band of process lines show the psychrometric conditions that would prevail with the designated rates of ventilation in air as it leaves the occupied space. Process lines associated with nonuniform or "varistate" environments are most realistic for ventilating systems that provide little or no air distribution.

If ventilating air enters a shelter directly from the atmosphere through a few openings, the environment near these points of entry will not differ greatly from the outside temperature. During winter weather part of the space may very cold. This objectionable situation can be avoided by one of three alternative methods, as follows:

- Provide reliable heating apparatus for warming the air before it enters the occupied space.
- Provide an extensive system of distribution ductwork and diffusion outlets.
- Use metabolic heat for tempering fresh air by arranging the ventilating system to recirculate part of the air that would otherwise be wasted.

Figure 8 relates paramaters associated with partial recirculation of air, including mixed and fresh air flow rates, fresh air temperatures, final air temperatures, and changes ir humidity ratio. This graphic information is based on a mixed air temperature of 50°F, which conforms to the prescribed minimum temperature for a shelter environment.

Recommendations

The following recommendations are made with regard to environmental problems in shelters:

- Concepts for shelter ventilating systems and components should be modified as necessary to provide for partial recirculation of air during cool and cold seasons.
- An evaluation should be made of parameters for partial recirculation of air during cold weather in shelters that have relatively large heat loads associated with lighting and heat transmission through shelter boundaries.
- Studies should be continued of interrelationships among population density, metabolic heat transfer, and the thermal environment in shelters to develop a more definitive correlation of significant parameters, including structural configuration and ambient effects, as well as metabolic and physiological factors.

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Appendix A

NUMERICAL TABULATION OF METABOLIC PARAMETERS

Some basic results of the study of processes for transfer of metabolic heat and moisture are compared graphically in Figures 4, 5, and 6 of Section II, Metabolic Parameters. In addition to the plotted data, computations were made for other conditions in the man/environment system. These supplementary results, as well as abridged tabulations of the plotted data, are shown in Tables A-1 through A-10 at the end of this appendix. Table A-1 is a key to identification of parameters that vary among the several tables in this group. Table A-3 represents the data from which all curves in Figures 4, 5, and 6 were plotted. Table A-4 represents supplementary values for the rows of dots on the figures. The computations for these supplementary values include a factor for the effect of clothing in attenuating vapor pressure differentials that cause diffusion through dry skin. Values of input parameters that remain constant in all tables, together with associated symbols used in the computer program, are as follows:

Barometric pressure, P8 = 1.0 atmosphere

Body temperature, $T7 = 37^{\circ}C$.

Metabolic rate, M = 100 kcal/hour

Total heat loss to environment, MO = 100 kcal/hour

Skin surface (DuBois area), $A = 2 \text{ m}^2$

Effective skin area, convection, A1 = 1.9 sq meters

Effective skin area, radiation, A2 = 1.3 sq meters

Radiation coefficient, Jl = 4.8 (absolute surface temperatures, $o_{K, are divided by 100}$)

Pulmonary ventilation, G = 0.6 Kg/hour of inspired dry air.

Tables A-2 through A-10 each contain eight columns of data. The first column, headed RHZ, shows the three values of relative humidity (Y2 = 0, 50, and 100 percent) for which computations were made at each value of air temperature. Each group of computations is id ntified by a subheading that includes the air temperature, $T^{O}C$, skin temperature, $T^{O}C$, and

the pressure of saturated water vapor, P3 mmHg, at skin temperature. Each of the other eight columns show two values of computed parameters for each value of relative humidity. These two parameters are identified by the upper and lower headings for each column. In column 2, LAHET is the latent heat loss, L kcal/hr, and SEHET is the sensible heat loss, S kcal/hr. In column 3, LHMIN is the minimum latent heat transfer, LO kcal/hr, associated with respiration, L3 kcal/hr, vapor diffusion through dry skin, L7 kcal/hr, and a spontaneous sweat, L4 kcal/hr, associated with physical activity. For sedentary activities, L4 = 0. Also, in column 3, STORE is the rate of heat storage, X6 kcal/hr, which vanishes when thermal equilibrium is attainable in the environment. In column 4, LREOD is the aggregate latent heat loss, L6, required to maintain thermal equilibrium, except that an alternative quantity is printed in place of LREQD when clothing is worn. This alternative quantity is equal to the metabolic rate minus the sensible heat loss that would occur if clothing were not worn. The quantity RADIT is sensible heat transfer by radiation, R1, from exposed surfaces of skin or clothing. In column 5, LHMAX is the maximum value of latent heat loss, L9, when all skin surfaces are wet, except that the value printed for LHMAX is the same as the value for LHMIN in column 3 when clothing is worn. The quantity, CONSK, is sensible heat transfer by convection, C1, from exposed surfaces of skin or clothing. In column 6, LHRES is the latent heat transfer, L3, and CORES is the sensible heat loss, D3, associated with respiration. In column 7, LHDSK is the latent heat loss, L2, associated with vapor diffusion through dry skin, and PMMHG is the partial pressure of water vapor in the environmental air in millimeters of mercury. In column 8, LHWSK is the latent heat loss associated with evaporation of sweat, E5, at wet skin surfaces, and CLOSR is the thermal resistance of clothing, K2, in clo units. In column 9, WETLR is a ratio, R5, relating to the proportionate area of wet skin and is defined as the ratio of actual heat loss associated with evaporation of sweat from wet skin surfaces to the maximum perspiratory heat loss when skin surfaces are completely wet. The quantity, CLODT, is the temperature gradient from skin to exposed surfaces of clothing.

The BASIC program used for computing and tabulating metabolic data associated with the simultaneous effects of all heat-mass transfer processes is reproduced in Table A-10.

TABLE A-1 DATA FOR NUMERICAL TABLES OF METABOLIC PARAMETERS

TABLE NUMBER	A-2	A-3	A-4	A-5	A-6	A-7	A-8	A-9	A-10
SKIN TEMPERATURE, T3, AT AIR TEMPERATURE, T, (CELSIUS) T3=34 T3=34+1.5"ATN(0.1967"(T-31))	×	×	×	×	×	×	×	×	×
ATTENUATION FACTOR, F3, FOR VAPOR DIFFUSION THROUGH CLOTHED SKIN AREAS F3=1.0 F3=1/(1+0.1%K2)	×	×	×	×	×	×	×	×	×
MEAN RADIANT TEMPERATURE, Ti, IN OCCUPIED SPACE (CELSIUS) T1=T T1=T3 OR T1=T2 T1=(T3+T)/2 OR T1=(T2+T)/2	×	×	*	×	×	×	×	×	×
CONVECTION COEFFICIENT, H1, FOR EXPOSED SKIN OR CLOTHING KCAL/(HR*SQ M*°C)	4.0	4.0	0.4	w .t.	0,	7.0	4.0	4.0	4.0
EVAPORATION COEFFICIENT, E1, FOR WET SKIN AREAS KCAL/(HR"SQ M"MMHG)	0.8	8.0	8	8.	10.0	14.0	8.0	8.0	8.0
RELATIVE AIR VELOCITY. VI CENTIMETERS/SECONI: FEET/MINUTE	15	15 30	15	10 20	23 45	45 90	15 30	15 30	15 30

(CELSIUS) T3=SKIN TEMPERATURE, T2=CLOTHING TEMPERATURE, T=AIR TEMPERATURE K2=THERMAL RESISTANCE OF CLOTHING (CLO UNITS)

TABLE A-2
METABOLIC PARAMETERS, SEI 1

DU#	LAUCT	LUMTAL	LREOD	LHMAX	LHRES	LHDSK	LHWSK	WETLR
RHZ	LAHET SEHET	LHMIN STØRE		CONSK		PMMHG	CLØSR	
	04							
AIR	TEMP: +1		SKIN: 34.					. 0. 0000
0	+35+5		-239.5	+35.5	+8.93	+26.5	-	+0+0000
	+64.5	+0.0	+26.6	+35-1	+2.80	+0.00	+3.520	
50		+31.5			+8.02	+23.5	+3.269	+0.0000
	+68.5	+0.0			+2.93	+4.50		+0.0000
100	+27 • 5	+27 • 5		+27.5	+7.12	+20•4 +9•20	+3.045	
	+72.5	+0+0	+30.0 SKIN: 34.	+39.4	+3.05		+3•0-3	. 201020
	TEMP: +2		-102·4	+36.0	+9+48	, +26•5	+0.0	+0.0000
0	+36.0	+36•0 +0•0	+28+6	+33.9	+1.48	+0.00		+10-196
50	+64.0 +28.3	+28.3		+28.3	+7.64	+20.7		+0.0000
30	+71.6	+0.0	+32.1	+37.9	+1.67	+8.77	+1.455	
100		+20.7	-102-8	+20.7	+5.80	+14.9	+0.0	+0.0000
	+79.3	+0.0	+35.5	+41.9	+1.86	+17.53	+1.239	+9.095
AIR	TEMP: +		SKIN: 34.			3		
0	+36.3	+36•3	-31.5	*36.3	+9.76	+26.5	+0•0	+0.0000
•			+29 • 6	+33.3	+0.81	+0.00	+0.832	
50		+25.9	-31.7	+25.9	+7.23	+18.6	+0•0	+0•0000
		+0.0	+34.4	+38.6	+1.05	+11.88	+0.608	
100	+15.4	+15.4	-32.0	+15.4	+ 4 • 67	+10.7		+0.0000
	+84.6	+0.0	+39+3	+43.5		+23.76	+0.438	+3.461
AIR	TEMP: +:		SKIN: 34					
0	+36•4	+36.4	-2.7	∜3 €∙ स		+26.5		+0.0000
	+63•6	+0.0	+30.0	+33.1	+0.55	+0.00		+2.849
50		*24.7	-2.9 +35.5	+24.7	+7.01	+17.6		+0.0000
	+75.3	*0.0	+35+5	+39.0		+13.37	+0.285	+0.0000
100		+12.9	-3.2	+12.9 +45.0	+4.10	+26.74		+1.167
	+87 • 1	+0.0	+41.1 SKIN: 34	+45•U	+1.06		+01143	
	TEMP: +		501141 34	+36.5	410.00	+26•5	+0.0	+0.0000
0		+36.5 +0.0		+32+8		+0.00		+0.737
51	+63•4 +26•2	+23.3	+26•2	+385.0	+6.76	+16.4		+3.0079
3.1	+73.8	+0.0			+0.56	+15.02		+0.000
100	+25.9	+10.0	+25.9	+153.3	+3.46	+5.8		+0.1106
100	+74.1	-0.0	+35.3	+38.0	*0.84	+30.04	+0.000	+0.000
AIR	TEMP: +		SKIN: 34			G		
0	+55+8	+36.7		+616.7	+10.12	+25.7		+0.0330
•	+44.2	-0.0	+11.4	+88•8	+0.01	+0.00		+0.000
50	+55.5	+21.8		+356•9	+6•46	+13.8		+0.1006
	+44.5	+0.0	+21.4	+88•8	+0.31	+16.85	40.000	
100	+55•2	+6.9	+55.2	+97.1	+2.74	+1.9		+0.5359
	+44+8	+0.0	+21.4	+22.8	+0.62	+33.70	+0.000	+0.000
AIR	TEMP: +			•00 C 3	19.90 NMH	6	400 I	+0.1353
0	+115.4					+0.00	+0.000	+0.000
						+8+1		+0.3539
50	+115.0	+18+3		+291.7	+5.75 -0.16			+0.000
	-15.0	+0.0		-33.6	+1.02	+0.0	-34.6	+1.0000
100	-33.6	-33.6 +148.3		-7.6	+0.50	+42-18	+0.000	+0.000
A 1 12	-14.7 TEMP: +		SKIN: 34		9.90 MMH			
0	+191.5	+37.2		+617.2	+10.67	+19.5	+161+3	+0.2660
U	-91.5	-0.0		- 45 • 6	-1.19	+0.00	+0.000	+0.000
50	+190 • 6	+12.7		+190.6	+4.58	+0.0	+186.0	+1.0000
•	-91.0	+0.5		- 45 • 6	-0.75	₹27.67	+0.000	+0.000
100	-236.3	-236.3		-236.3	-1.74	+0.0		+1.0000
	-90.6	+426.9	-44.7	- 45 • 6	-0.29	+55.34	+0.000	+0.000
AIF	TEMP:		SKIN: 34		39.90 MM			
0	+381.7	+38+0	+381.7	+618.0	+11+45	+10.8		+0.5926
	-281.7	+0.0		-136.8	-2.79	+0.00	+0.000	
50	-169•6	-169.6		-169.6	+0.12	+0.0		+1.0000
	-881.0	+550.6	-142.1	-136.8	-2.08	+51-07	+0.000	+0.000

TABLE A-2 (CONCLUDED)

	_							
RH	Z LAHE	T LHMIN	LREOD	LHMA	(1.1155.0		
	SEHE	T STORE	DADUT	CHITAL	LINKES	LHDSK	LHWSK	WETLE
		• 51016	KHUN I	C9.4.24	CORES	PMMH (CLØSR	CL 001
	• • • • • • • •	_						4500
A.	IR TEMPT	+0.00	SKIA: 3	4.00 C	39.90 MM	u c		
(0 +34.9	+34.9	-370.5	+34.9	+8-41			
	+65.0	+0.1	1043	1040	70.41		+0.0	+0.0000
50			7244 /	+30.2	+4.12	+0.00	46 050	+30.896
•				+ 33+0	+8.01	+25.0	+0.0	+0.0000
	+67•0			+37.3	+4.21	A9. 20		+ 04 0000
100	3 +31+1	+31+1	-370.7	+31.1		+ 60 69		+30 - 763
	+ 68 • 9				+ 7. 61	+23.5	+0.0	+0.0000
Δ1	R TEMP:	* 1 F 00	720.2	+38.4	+4,29	+ 4. 58	+5.005	+ 30 - 632
		A 1 24 00	SKIN: 3	4.00 C	39.90 MM	H G		000000
Ç	+35.7	+35.7	~171.7	+ 35. 7	40 00			
	+64.2	+0.0	+27-6	424 S	+2.14 +7.90 +2.29	72003	+0• C	+0.0000
50	+30.2	+30.0	-121.0	13403	+2.14	+0.00	+2.617	+15.403
	A 40 0	+0.0	-171.9	+30.2	+ 7• 90	+22.3	+0.0	+0.0000
100	407+0	+0.0	+ 30 • 0	+37•5	+2.29	+6.39	+ 2. 2 Ac	115 000
100	+24.6	+24.6	-172.0	+24.6	+6.59	1100	* CO 340	+15-009
	+ 75 • 4	+0.0	+32.5	4.40.4				+0.0000
AI	R TEMP:	+23.00	CVINA	¥ 4U# 4	72.45	+12.78	+2.115	+14-610
ō	436 0	+23.00	27141 34	100 C	39.90 MMH	ł G		• • • • •
•		+20.5	- 60 • 1	436.2	+9 65	+26.5	40. n	
	703.8	+0.0	+29.2	+33.5	+1.08	10.00		+0.0000
50		+26.9	- 60. 3	+26 0	+1.08 +7.42 +1.29 +5.16	+0.00		+ 7- 055
	+73.0	40.0	400	720. Y	+ 7. 42	+19.5	+0.0	+0.0000
100		10.0	73344	+ 38 • 3	+1.29	+10.53	+0.940	+6.393
100	+1/0/	+17+7	-60.5 +37.7	+17.7	+5.16	+12.5		+0.393
	+82.3	+0+0	+ 37. 7	+ 43 - 1	+1.51	124 5		+0.0000
AI.	R TEMP:	30.00	SKIN. 24	-00 0	41.21	+21.07	+0•749	+5.730
0	+41.1	+36.6	21111 34	•00 6	19•90 MMH	'G		
-	A 50 0						44.7	
	- 38 • 9	+0+0	+28 • 4	*30·4	+0.15	+0.00	10.000	+0.0011
50	+ 40 • 8	+0.0 +22.6 +0.0 +8.5	+ 40 · 8	+371.2	+10.06 +0.15 +6.62 +0.43 +3.11	+0.00		+0.000
	+59.2	+0.0	4 90 A	100	¥0.05	+15-1	+19.1	+0.0523
100	+ 40 - 5	10 6	1 40 4	+30.4	+0•43	+15.91	+0.000	+0.000
	+59.5	¥0+3	+ 40 • 5	+125.9	+3.11	+3.0	+33+5	. 0 0 0 0 0
			+28.4	+125.9	+0.73	+31.83	1 330 3 1	0.2727
A11	<pre> < TEMP: + </pre>	33,00	SKIN: 3A.	አሰበ ድ ሳ	0 00		+0.000	+0.000
0	+85.5	+36.8	105 E		+10.24 -0.25	เ		
	+14.5	-0.0	70303	7010.8	+10-24	+24.3	+50.9	0.0830
50	105	-0.0 +20.1 -0.0 +3.4 +49.9	+ 7• 2	+ 7• 6	-0.25	+0.00	+0.000	100007
30	-03-1	+20-1	+85.1	+325.9	+6.13	+11.0	-0.000	+0.000
	+14.9	-0.0	+7.2	+7.4	40.03	411.0	+ 68 • 0 +	0.2126
100	+34.9	+3.4	4 P A . W		70.07	+18.87	+0.000	+0.000
	+15.0	+49.9	70400	+34.9	+1.92	+0.0	+33.0 +	1.0000
Ato	TCMO	7 49.9	+ 7• 2	+ 7.6	+0.41		40.000	10000
717	ICHPI +	37.00 S	KIV: 34.	00 C 3			+0.000	*0.000
0	+145.6		+145.4	4617.0	110 40	,		
	~ 45. 6	+0.0	- 22 0	. 01 700	-0.78 +5.33 -0.40	+21.6	+113.6 +	0.1872
50	+145.2	416.0	- 46.0	-55-8	-0.78	+0.00	+0.000	+0.000
••	- 45 0	+16.2	+ 1 45• 2	+254.1	+5.33	+5.0	+ 1 3 4 0 1	0.000
	- 45. 2	+0.0	-22.0	-22.8	# D. AO	402 54	+134.9 +	0.5423
100	-109.0	-109.0	+144.8	-109.0	+ 0 - 00	723034	+0.000	+0.000
	- 44.8				+0.00	+0.0	-109.0 +	1.0000
ATR	TEMP: +		-22.0	-55.8	+0.00	4 A T. OO	+0.000	+0-000
	1010		KIN: 34.	00 C J9	POU WARV			. 04 000
U	¥ 637 • 4	+37.5	+269•4 -	+617.5	+10.99	415.A		
	-169.4	+0.0	-83.0	-93.4	+10.99 -1.85 +3.05	+ 1 a+ y	+242.5 +	0•3998
50	+63.2	+5.7	1262 0	-03.0	-1.85	+0.00	+0•000	+0.000
	-168.9	+00E #	- 200 • 9	+63.2	+3.05	+0.0	+60.1 +	1.0000
ATD	TCHO.							
WIK	TEMP: +5		(IN: 34.0	00 C 39	•90 MMHG	. 00075	********	•0•000
0	+349.2	+37.9	349.2	6617.0	* * * * * * * * * * * * * * * * * * * *			
	-249.2		106 1	01 100		+12.3	+ 325.6 +0	0.5368
50			125.1 -	121.6	~ 2 • 52		0.000	0000
		-95.8	348.6	-95.8	+1+05		-0000	0.000
	-248.6	+ 444.A -	125.1 -	121.6		+0.0	-96.9 +1	1.0000
AIR	TEMP: +6		1N. 24 0		-1.5/	46.28	+ 0000 +0	0.000
0			F . A -	, U G 39	90 MMHG			
_		* VO + D +	514.8 +	618.5	+12.00	+4.7 +	498.0	
	-414.8	+0•0 ~	213.3 -	197.6	-3.87		498.0 +0	1128 W
AIR	TEMP: +7	0 • 00 SK	IN: 34.0	0 0 30	9U MMHG	+0.00	·0•000 +	0.000
0	+619.2		400.	(10 0	YU MMHG			
	- 588 • 6	140 1	688.6 +	014.5	12.71	+0.0 +	606.5 +1	• 0000
Atm .	704D	+69.4 -	304.8 -	273.6	-5.21	+0.00	0.000 +	0.000
WIK .	157P1 +8	U+00 Sx	IN: 34.0	D C 20	00 4444	J- JU +	U+ UUU +	0.000
0 .	• 620• O	+40.0 +	871.3 +	690.0				
	771.3	251.3 -	415. O	040 4	13.47	+0.0 +	606+5 +1	• 0000
			41308 "	349.6	- 6. 57			0.000
						-		

TABLE A-3
METABOLIC PARAMETERS, SET 2

RH%	LAHET SEHET	LHMIN STØRE	LREGO THDAS		LHRES CØRES	L HDSK PMMHG		WETLR CL ØDT
ATD	TEMD. A	10.00	SKIN: 32	.00 C 29	5. 47 MMU	c.		
0			-210.0			+23.7	+0-0	+0.0000
·	+67.3	+0.0	+27.9	+36.6	+2.80	+0.00		+18.289
50	+28.7	+28.7	-210-1	+28.7	+8.02	+20.7		+0.C000
••	+71.3	+0.0	-210·1 +29·6	+38.8	+2.93	+4.60	-	+18.004
100	+24.7	+24.7	-210.2	+24.7	+7.12	+17.6		+0.0000
	+75.3	+0.0	-210•2 +31•2	+24.7 +41.0	+3.05	+9.20		+17.718
AIR	TEMP: +	20.00	SKIN: 32	29 C 3	6.26 MMH	G		
0	+33.6	+33.6				+24.1	+0.0	+0.0000
	+66•4	+0.0	+29•7 -77•4	+35.2	+1.48	+0.00	+1.334	+8.209
50	+25.9	+25• 3	-77•4	+25.9	+7.64	+18-3		+0+0000
	+74.0	+0.0 +18.3	+33•2 -77•6	+39.2	+1.67	+8.77		+7 • 657
100								+0.0000
		+0.0		+43.2		+17.53	+0.938	+7.099
	TEMP: +		SKIN: 32					
C	+34.4	+34+4	-12.3 +30.5	+34.4	+9.76	+24.7	-	+0.0000
50	+03+3	+0.0	-10-5	*34.3	+7.02	+16.8		+0.0000
30	+74.0	+24.0 +0.0	-12.5 +35.3	+24.U	+1.05	411.88		+2+680
100	413.5	113.5	-19.7	413.5	+4.67	+8.9		+0.0000
ioo	486.A	+0.0	-12.7 +40.2	+ 44.9	+1.28	+23.76		+1.927
AIR	TEMP: +	27.00	SKIN: 33	.00 C 3	7.73 MMH	6		
0	+35.0	+35.0	+12-1	+35.0	+9.88	+25.1	+0.0	+0.0000
•	+65.0	+0.0	+30.7	+33•B	+0.55	+0.00		+1.673
50	+23.2	+23.2	+30.7 +11.9 +36.2 +11.6	+23.2	+7.01	+16.2	+0.0	+0.0000
	+76.8	+0.0	+36.2	+39.7	+0.80	+13.37	+0.115	+0.830
100	+11.6	+11.4	+11.6	+171.2	+4.10	+7.3	+0.2	+0.0013
	+88•4	+0.0	+41.7	÷ 45 • 6	+1.06	+26.74	+0.000	+0.000
	TEMP: +	29.00	SKIN: 33	•44 C 3	8.67 MMH			
0	+35.7	+35.7	+34•8 +30•8	+35.7	+10.00	+25.7		
	+64.3	+0.0	+30-8	+33.2	~0∙28	+0.00		+0.071
50	+34.5	+22.5	+34•5 +31•2	+366.2	+6.76	+15.2		+0.0349
			+31.2	+33.7	+0.56	+15.02	+0.000	+0.000
100	+34.2 +65.8	+9•2 +0•0	+34.2	+134.6 +33.7	+3•46 +0•84	+4.6 +30.04		+0.1994
ATR	TEMP: +			. OD C 3	40.04 UMM 00.0		+0.000	+0.000
0				+616.7			+20.0	+0.0330
U	+55.8 +44.2 +55.5	-0.0						+0.000
50	+55.5	+21.8		+356.9	+6.46	+0.00 +13.8		+0.1006
	+ 44.5	∔ ∩∩	+21.4	+22.8	+0.31	+16.85	+0.000	
100	+55.2	+6.9	+21 • 4 +55 • 2	+97 • 1	+2.74	+1.9	+50.5	+0.5359
	+44.8	+0.0				+33.70	+0.000	+0.000
AIR			SKIN: 35					
0	+100.5	+38•4	+100.5	+651.5	+10.36	+25•2		+0.1013
	-0.5	+0.0	-0.0		-0.52			+0.000
50	+100.2	+19+8		+326-3	+5.75	+10.3		+0.2622
	-0.2	-0.0	-0.0	-0.0	-0.16	+21.09	+0.000	+0.000
100	+1.0	+1.0	+99•8	+1.0	+1.02	+0+0		+1.0000
ATD	+0.2	+98.8	-0.0	-0.0	+0.80	+42.18	+0.000	+0.000
	TEMP: +	+39.6	SKIN: 35	• 35 C 4 • 672• 9	3.56 MMH		.124 1	+0 2025
0	+167.9	+0.0	+167•9 -33•1	-33.6	+10.67	+23•1 +0•00	+0.000	+0.2025
50	+167.4	+15.2	+167.4	+246.2	+4.58	+3.6		+0.6591
50	-67.4	+0.0	-33-1	-33.6	-0.75	+27.67	+0.000	+0.000
100	-180.7	-180.7	+167.0	-160.7	-1.74	+0.0		+1.0000
	-67.0	+347.7	-33.1	-33.6	-0.29	+55.34	+0.000	+0.000
AIR	TEMP: +		SKIN: 36		4.57 MMH			
0	+351.9	+41 - 1	+351.9	+688.9	+11.45	+15.4	+325.0	+0 • 47 97
	-251.9	+0.0	-127.5	-121.6	-2.79	+0.00	+0.000	+0.000
50	-98.7	-98.7	+351.2	-98.7	+0.12	+0.0		+1.0000
	-251.2	+449.8	-127.5	-121.6	-2.08	+51.07	+0.000	+0.000

TABLE A-3 (CONCLUDED)

RH%	Lahet Sehet			LHMAX CØNSK	LHRES CORES	LHDSK PMMHG	LH WSK CLØSR	WETLR CLØDT
ATE	TEMP.	+C-00	SKIN: 31	. go r	25 44 441			
Ç.	+32.0	+32.0			33• 44 MMH +8• 41		+0-0	+0.0000
_	+38.0	+0.0	+ 25. 9	+38.0	+4.12	+0.00		+28-490
50	÷30•1	+30•1	-339 • 4	+ 30 • 1	+8.01	+22.0		+0.0000
	+69.9	+30·1 +0·0 +28·1 +0·0	+26.7	+ 39 • 1	+ 4. 21	+2•29	+ 4• 553	+28.356
100	*28 • 1	+28+1	-339.5		+ 7• 61			+0.0000
ATR	TEMP:	+U+U +15.00	+27.4 SKIN: 32	+ 4U+ 1	+ 4+ 29	+ 4+ 58	+ 4• 409	+ 58 • 555
0	+33.1	+33-1	-143.7	+33.1	•9•20		+0-0	+0.0000
_	+66.9	+0.0	+28.8	+35.9	+2.14	+0.00		+13-213
50	+27.5	+27.5	+28 • 8	+27.5	+7.90	+19.6	+0.0	+0.0000
	+72.4	+0.0 +21.9	+31.3	+38+9	+2.29 +6.59	+ 6 • 39	+1.927	+12.814
100				+21.9				+0.0000
ΔΙΡ	TEMP	+0.0	+33.7			+12.78	+1 • 733	+12.411
o non	+34.0	+34.0	37. g	433.0	36 67 MMH	+24.4	40.0	
•	+65.9	+0.0	-37.8 +30.2	*34.7	+1.08	+0.00	+0.841	+5.295
50	+24.8	+24.8 +0.0	-38.0	+24.8	+7.42	+17.4		+0.0000
		+0•0	- 38 • 0 + 34 • 5	+39 • 4	+1.29	+10.53		+ 4. 629
100	+15.5	+15-5	- 38 • 2 + 38 • 7	+15.5	+5.16	+10.4	+0+0	+0.0000
ATD	+84.4	+0+0	+38.7	+44.2	+1.51	+21.07	+0-504	+3•960
0	+ 45.4	+36.2	SKIN: 33	11 G G				
•	+54.6	+0.0	+26.3	+28.2	+0.15	+25.7	+0-000	+0+0162
50	+ 45 • 1	+0.0 +22.1 -0.0	+ 26 • 3 + 45 • 1	+361.5	+ 6 • 62	+14.5	+24.0	+0.0677
	+54.9	-0.0	+ 26• 3 + 44• 8	+28.2	+0.43	+15.91	+0.000	+0.000
100			+ 44.8	+116-1	+3-11	+3.3	+ 38 • 4	+0.3402
ΔŧΒ	+55.2	+0+0		+28+2	+0.73	+31.83	+0.000	+0.000
0	+77.1	+37.6	SKIN: 34	********	41017 MMH			. // 0.660
•	+22.9	-0.0	+11.3	+11.9	-0.25	+25+6 +0-00	+0.000	+0.0660
50	+76.8	+21.0	+11.3 +76.8 +11.3	+345-1	+ 6.13	+12+3	+ 58 • 4	+0.1722
	+23.2	-0.0	+11.3 +76.3	+11.9	+0.07	+18-87	+0.000	+0.000
100	+54.2	+ 4. 2	+ 76. 3	+54.2	+1.92	+0.0	+ 52 • 2	+1.0000
ATD	+ EJ • 0	72203	71103	-11.4	+0.41	+37•73	+0.000	÷0•000
0	+126.2	+39.0	*126.2	30 € 4 4449. A	12.89 MMH	G 	404.0	
•	-26.2	-0.0	-12.5	- 12.0	- O. 70	40.00	+0.000	+0+1399
50	+125.6	+18.2	+125-8	+299.5	÷ 5 • 33	+7.9		+0.3827
	-25.8	+0.0	-12.5	-12.9	-0.40	+23-54		+0.000
100	-63.6	° 63• 6	+125•4	- 63• 6	+0.00	+0•0	- 63 • 6	
ATD	*25.4	+189+1	-12.5	-12.9	+0.00	+ 47• 08	+0.000	+0.000
e	+242.1	+ 40 · A	SKIN: 35.	83 U 4	14.17 MMH	5		
•	-142-1	+0.0	+242.1 -70.6 +241.5	- 69. 7	-1.85	+0°00 1 +02+	+510+3	+0+3142
50	+127.9	+8+5	+241+5	*127·9	+3.05	+0.0	+124.9	+1.0000
			~ 70.0	- 07 • /	-1.32	+33.95	+0.000	+0.000
	TEMP: +		SKIN: 35.	96 C 4	4. 48 MMH	3		
0	+319.9	+ 40 • 9	+319.9	+ 68 7 • 4	+11.31	+16.8		+0.4315
50	-26.5		-110.7 +319.3			+0+00	+0.000	+0.000
-	-219.3	+345.5		-26.2 -106.7	+1.06 -1.87	+0+0		+ 1 • 0000
ATR	TEMP: +		SKIN: 36.		4.81 MMH	+ 46 • 28 3	+0.000	+0.000
0	+ 483 • 5				+12.00	+9•6	+461.9	+0.6783
A	-383.5		-198.0	-181.7	-3.87	+0.00		+0.000
	TEMP: +		SKIN: 36.					
0	+656·4 -556·4			+696+2		+1.8	+641.9	
AIR	TEMP: +1		-294.0 SKIN: 36.	-257•2		+0+00	+0.000	+0.000
	+698 • 5				+13+47	, +0•0	+695•0	1.0000
	- 738 • 5			- 332• 9	-6.57	+0.00	+0+000	+0•000

TABLE A-4
METABOLIC PARAMETERS, SET 3

RHZ	LAHET		LREQD	LHMAX	LHRES	L.HD.SK	LHWSK	WETLR
	SEHET	STØRE	RADHT	C ØN SK	CØRES	PMMHG		
							OLOSIN	CL OD I
	TEMP:	+10.00	SKIN: 32	2.00 C 3	35 67 MMH	ខេ		
0	+27.6	+32.6	-210.0	+32.6			+0.0	+0 0000
	+72.4	+0.0	+30.1	+39.5	+2.80	40.00	+0.714	+17.914
50	+24.5	+28.7	-210-1	+28.7	48.00	+16.4	72.716	+1/+914
	+75.5			+ 41. 2	+0.02	71004	+0.0	+0.0000
100	+21.3		-210.2	+24.7	12.10	+4.60	+2.571	+17 • 689
	+78.7	+0.0					+0.0	+0.0000
ATR		+20.00		+42.9	+3.05	+9.20	+2.436	+17.461
0	+30.9			. 29 0 3	6.26 MMH	G		
•		+33+6	-77.2	+33.6		+21.4		+0.0000
50	+69•1	+0.0	+31.0	+36.6	+1-48	+0.00	+1.250	+8.010
30		+25.9	-77.4	+25.9	+7.64	+16.5	+0.0	+0.0000
	+75.8	+0.0	+34.0 -77.6	+40-1	+1.67	+8.77	+1.071	+7 - 525
100	+17.2		-77.6	+18.3	+5.80	+11.4	+0.0	+0.0000
	+82.7	+0.1	+37.2	+43.7	+1.86	+17.53	+0.916	+7.023
AIR	TEMP: 4	25.00	SKIN: 32	•70 C 3	7.10 MMH	G		. , . 020
0	+33.2	+34.4	-12.3	+34.4	+9.76	+23.A	±0.0	+0.0000
	+66.8	+0.0	+31.1 -12.5	+34.9	+0.81	10.00	+0.50	+0.0000
50	+23.4	+24.0	-12.5	+24.0	±7.22	+14.0	+0.534	+3,337
	+76.6	+0.0	-12.5 +35.6	4 70 D	+1.05	410.2		+0.0000
100	+13.3	+13.5	-12.7	+37+7	+1.05	+11.88	+0.368	
;	+86+6	10.0	+40.3	+13.5 +45.0	+4.67			+0.0000
ΔTD		-07 00	T40+3	+45.0	+1.28	+23.76	+0.236	+1.912
0	+34.3	-27.00	SKIN: 33	•00 6 3				
U	43443	+35.0	+12.1	₹35.0	+9.88	+24.4	+0.0	+0.0000
	765.7	+0.0	+31.0	+34.1	+0.55	+0.00	+0.263	+1.624
50	+23.0	+53.5	+31.0 +11.9 +36.3 +11.6	+23.2	+7.01	+16.0	+0.0	+0.0000
	+76.9	+0.0	+36•3	+39.8	+0.80	+13.37	+0.113	+0.817
100	+11.6	+11.4	+11.6	+171.2	+4.10	+7.3		+0.0013
	70044	70.0	+41.7	+45.6	+1.06	+26.74	+0.000	+0.000
		29.00	SKIN: 33	.44 C 3	9.67 MMH	G		
0	+35.7	+35.7	+34.8	+35.7	±10.00	+25.7	+0.0	+0.0000
	+64.3	+0.0	+30.8 +34.5	+33.2	+0.28	+0.00	+1.011	+0.066
50	+34.5	+22.5	+34.5	+366.2	+6.76	+15.2	+12.5	+0 +0 +0
	+65.5	-0.0	+34.5 +31.2	+33.7	*0.56	+15.02		
100	+34.2	+9.2	+34.2	+134.6	+3.46	+4.6		+0.000
•	+65.8	+0.0	+31.2		+0.84			+0.1994
AIR			SKIN: 34	.00.0	*******	+30.04	+0.000	+0.000
0	+55.8	+36.7	+55.8	• 00 0 3	7. 70 MMH			
•	+44.2	-0.0	+01.4	+010+7	+10.12	+25.7	+20.0	+0.0330
50	155.5	-0.0 +21.8 +0.0	+21.4	+22.8	+0.01 +6.46	+0.00	+0.000	+0.000
50	+33+3	741.0	+55.5	+356.9	+6.46	+13.8	+35.3	+0•1006
100	+55.2	+0.0	+21.4	+55.8	+0.31 +2.74	+16.85		
100			* JJ• 2	+97 • 1	+2.74		+50.5	+0.5359
4.5	+44.8	+0.0	+21.4	+55*8	+0.62	+33.70	+0.000	+0.000
	IEMPI +	35.00	SKIN: 35	∙00 C 48	2.18 MMH(3		
0	+100.5	+38.4	+100.5				+65.0	+0.1013
	-0.5	+0•0 +19•8	-0.0		-0.52	+0.00	+0.000	+0.000
50	+100.2	+19•8	+100.2	+326.3	+5.75	+10.3		+0.2622
	0.2	-0.0	-0.0	-0.0	-0.16	+21.09	+0.000	+0.000
100	+1.0	+1.0	+99.8	+1.0	+1.02	+9.0		1.3000
	+0.2	+98.8	-0.0	-0.0	+0.20	+42.18	+0.000	+0.000
AIR	TEMP: +	40.00	SKIN: 35		3.56 MMH			.0000
0	+167.9	+39.6	+167.9	+672.9	+10-67	+23.1	+134-1	.0.2025
	-67.9	+0.0	-33.1	-33.6	-1.19	+0.00	+0.000	
50	+167.4	+15.2	+167.4	+246.2	+4.58	+3.6		+0.000
-	-67.4	+0.0	-33.1	-33.6	-0.75	+27.67	+159.2	
100	-180.7	-180.7	+167.0	-180.7			+0.000	+0.000
	-67.0	+347.7			-1.74	+0.0	-178.9 +	
ΔYD	TEMP: +		-33.1	-33.6	-0.29	+55•34	+0.000	+0.000
	+351.9		SKIN: 36.		1.57 MMHG			
		+41+1	+351.9		+11.45	+15.4	+325.0 +	
	-251.9	+0.0	-127.5	-121.6	-2.79	+0.00	+0.060	+0.000
50	-98.7	-98.7	+351.2	-98.7	+0.18	+0.0	-98.8	1.0000
	-251.2	+449•8	-127.5	-121.6	-2.08	+51.07	+0.000	+0.000

TABLE A-4 (CONCLUDED)

RHZ	LAUCT	LUMTU	LDCAD	LUMAY	Lupce	LHDev	. uuez	meas o
Kn 4			L REQD RADHT		LHRES			WETLR CLØDT
	36461	21046	KHONI	00 151	OURCS	F-1-11-10	OCOSK	02001
AIR	TEMP:	+0.00	SKIN: 31	89 6 3	5.44 MMH	G		
0	+25.0			+32.0			+0.0	+0.0000
	+74.9	+0.0			+4.12			+27.982
50	+23.7	+30+1	-339 • 4	+30-1	+5.01	+15.7		+0.0000
	+76.3	+0.1	+29 • 3	+ 42 • 8	+4.21	+2.29	+4.082	+27.889
100	+22+3	+28 • 1	-339•5	+28 - 1	+ 7- 61	+14.7	+0•0	+0.0000
	+77.7	+0+0	+29.8	+ 43 • 6	+ 4.29	+ 4+ 58	+3.995	+27.792
		15.00	SKIN: 32					
0	+29 • 1	+33-1	-143.7	+33-1	+9•20	+19-9		+0.0000
	+70+8	+0.0	+ 30 • 6		+2+14			+12.921
50		+27.5	-143.9	+27.5	+7.90	+16.6		+0.0000
	+75.5	*0•0	+32+6		+2.29			+12.588
100	+19+8	+21.9	-144-1			+13.2		+0.0000
A 1 D	+80.2	+0.0	+34.7	+ 43 • 1	+2,45		+1.005	+12.245
0	+32.2	23.00 +34.0		+34.0		+22+5	A 0 - 0	+0.0000
U	+ 67.8		+31+1			+0.00		+5-158
50	+23.8	+24.8	-38.0			+16.3		+0.0000
30	+76.2	+0.0	+35.0			+10.53		+ 4. 549
100	+15.1	+15.5	-38.2		+5.16	+9.9		+0.0000
	+84.9	+0+0	+39+0	+ 44. 4	+1.51	+21.07		+3.925
AIR	TEMP: +		SKIN: 33				•	•
0	+45.4	+36.2			+10.06	+25.7	+9.7	+0.0162
	+54.6	+0+0	+26.3	+28 • 2	+0.15	+0+00	+0.000	+0.000
50	+45.1	+22 • 1	+ 45 • 1		+6.62	+14.5	+24.0	+0.0677
	+54.9	-0.0	+26.3	+28.2	+0+43	+15.91		+0.000
100	+44.8	+8 • 1	+ 44+8	+116+1	+3.11	+3.3		+0.3402
	+55+2	+0+0	+26.3	+28.2	÷0•73	+31-83	+0.000	+0.000
		33.00	SKIN: 34	56 C 4	1 · 1 7 MMH	G		
0	+77•1	+37.6	+77-1 +11-3	+636+0	+10.24	+25+6		+0.0660
	+22.9		+11.3	+11+9	+0.25			+0.000
50		+21+0	+76+8 +11+3	+345+1	+6+13	+12+3		+0.1722
100	+23·2 +54·2	-0.0		+54.2		+18+87		+0.000 +1.0000
100	+23.6	+22.3	+11+3	+11.9	+0.41	+37.73		+0.000
AIR	TEMP: 4	37.00		30 C 4	2.89 MMH		. 00000	. 0000
0	+126-2	+39+0	+126-2			+24.5	+91+2	+0-1399
_	-26.2	-0-0	-12.5					+0.000
50	+125-8	+18.2	+125.8			+7.9	+112.6	+0.3827
	-25.8	+0•0	-12.5	-12.9	-0.40	+23.54	+0.000	+0.000
100	-63•6	-63.6	+125.4	-63.6	+0.00	+0•0	- 63 • 6	+1.0000
	-25.4	+189+1		-12.9	+0.00	+ 47•08	+0.000	+0.000
		45.00	_					
0	+242-1	+ 40 • 4	+242-1	+682.3	+10.99	+20-1		
	• 142• 1	+0+0			-1.85			+0.000
50	+127.9	+8+5		+127.9		+0.0		+1.0000
410			- 70 - 6				+0.000	+0.000
0	+319.9	+ 40 • 9		+ 687• 1		+16.8	A 201 . Q	+0.4316
U	-219.9	+0.0	+319•9 -110•7			+0.00		+0.000
50		-26-2			+1.06	+0•0		+1.0000
30		+345.5	-110-7			+ 46 • 28	+0.000	
AIR	TEMP: +		SKINE 36					0.000
0	+483+5	+41+8	+ 483 • 5		+12.00	+9.6	+461.9	+0.6783
-	-383-5	+0+0	-198-0	. 181.7	-3.87	+0.00		+0.000
AIR	TEMP: +		SKIN: 36					
0	+656.4	+ 42 • 6	+656+4	+696.2	+12.71	+1.8	+641.9	+0.9391
	-556-4	+0.0	-294.0	-257.2	-5.21	+0.00	+0.000	+0.000
	TEMP: 4		SKIN: 36					
0	+698+5				+13-47	+0.0		+1.0000
	-738 • 5	+140+1	-399•1	-332.9	~6.57	+0+00	+0.000	+0+000

TABLE A-5
METABOLIC PARAMETERS, SET 4

RH%	LAHET SEHET	LHMIN STØRE					LHWSK Cløsr	WETLR CL ODT
AFD	TEMP+ +	10.00	SKIN: 32	.00 C 3	5.67 MMH(3		
0	+27.7	+32.6		+32.6		+18.7	+0+0	+0.0000
•	+72-3	+0.0	+32.9	+36.6	+2.80	+0.00	+2.660	
50	+24.5	+25.7	-185.0	+28.7	+8.02	+16.5		+0.0000
	+75.4 +21.3	+0.0	+34•3 -185•1	+38.2	+2.93		+2.514	
100	+21.3	+24.7	-185-1	+24.7	+7.12	+14.2		+0.0000
	+78•6	+0+0	+35+8	+39.8	+3.05		+2.377	+17.026
AIR	TEMP: +		SKIN: 32					
0	+31.0	+33.6	-63-2	+33 • 6	+9.48	+21.5		+0.0000
	+69.0	+0.0	+33.7	+33+8	+1 • 48	+0.00		+7.618
50	+24.3	+25.9	-63.4	+25.9	+7.64	+16.3		+0.0000
		+0.0	+37.0	+37.0	*1·67	+8.77		+7.087
100	+17.3	+18-3	-63 • 6	418-3	+5.80	+11.5		+0.0000
		+0.0	+40 • 5	+40+4	71.00	+17.53	+0.033	+0.333
			SKIN: 32	.70 6 3	1/01U MMA	√23•6	40.0	±0.0000
0	+33.3	+34.4	-3•5 +33•7	+39.1	+9.76	+0.00		+2.946
60	+66.7		-3.7	+36+1	47.23	416.3		+0.0000
50	+23.5 +76.5	+24.0 +0.0	A28.7	A34.7	+7.23 +1.05	+11.58		424178
100	+13.4	+13.5	-3.9	413.5	+ 4. 67	+8.7		+0.0000
100	+86.6	+0.0		+ 41.5	+1.28		+0-171	
ATR		27.00	SKINE 33	.00 C 3	7.73 MMH			******
0	+34.5	+35.0		+35•0	+9.88	+24.6	+0.0	+0.0000
•	+65.5	+0.0	+33.6	+31.4	+0.55	+0.00		+1.238
50	+23-1	+23.2	+33+6 +18+7	+23.2	+7.01	+16.1	+0.0	+0.0000
•	+76.8	+4.0	+39 • 4 +18 • 5	+36.6	+0.80	+13.37	+0.049	+0.355
100	+18-5	+11.4	+18.5	+146.2	+4.10	+6.9	+7.4	+0.0523
	+81.5	+0.0	+41.7	+38.8	+1.06	+26.74	+0.000	+0.000
	TEMP: +	29.00	SKIN: 33	.44 C 3	38.67 MMH	G		
0	+39.8	+35.7	+39.8 +31.2	+509.6	+10.00	+25.5	+4.3	+0.0087
	+60.2	+0.0	+31.2	+28.7	+0.28	+0.00	+0.000	
50	+39.5	+22.5	+39 • 5 +31 • 2	+312.3	+6.76	+14•8	+18.0	
	+60.5	+0•0	+31.2	+28.7	+0.56		+0.000	+0.000
100	+39.3	09.2	+39 • 3 +31 • 2	+114.9	+3.46	+4-1		+0.2844
	+60.7	-0.0	+31-2	+28.7	+0.84		+0.000	+0.000
AIR	TEMP# 4	31.00	SKIN: 34	•00 C	39.90 MMH	G		
ð	*57.2	+36.7	+59.2	+525.7	+10.12	+25.3	+23.8	+0.0462
	+40+8	+0.0	+21 • 4 +58 • 9 +21 • 4 +58 • 6	+19.4	+0.01	+0.00	+0.000	+0.000
50	+58.9	451.8	+ 38 • 9	+304.3	* 0 · 40	+13.3	+0.000	+0.1314
	+41+1	+0.0	+61•4	+ 27 • 4	40.31	+10.03	454.4	A0.4804
100	+41.4	*O.7	+21.4	*10.4	+0.62	↑33.70	+0-000	+0.000
ATD	TEMP: 4	35.00	SKIN: 35	•00 C	42.18 MMH		.0000	
0	4100.5	+38-4	+100+5	+555.3	+10.36	+24.7	+65.5	+0.1202
•	-0.5	+0.0	+100+5 -0+0	-0.0	-0.52	+0.00	+0.000	+0.000
50	+100.2	+19.8	+100-2	+278.2	+5.75	+9.7	+84.7	+0.3110
•		+0.0	-0.0	-0.0	-0.16	+21.09	+0.000	+0.000
100	+1.0	+1.0		+1.0		+0.0		+1.0000
	+0.2	+98+8		-0.0	+0.20	+42.18	+0.000	+0.000
AIR	TEMP:	40.00	SKIN: 35	-58 C	43.56 MMH	IG		
0	+162.6	+39 • 6		+573 • 5	+10.67	+22+3		+0.2308
	-62.8	-0.0	-33-1	-28.5		+0.00	+0.000	
50	+162.4	+15.2	+162.4	+210.0	+4.58	+2.6		+0.7559
	-62.4	+0.0	-33-1	-28.5		+27.67		+0.000
100	-153.9	-153.9	+161.9	-153.9		+0.0		+1.0000
	-61.9	+315.8	-33.1	-28.5		+55.34	+0+000	+0.000
	TEHP:		SKIN: 36		44.57 MMH			.0 5051
0	+333.6	+41+1	+333 • 6	4587.3		+13.8		+0.5356
	-233-6	-0.0		-103-4		+0.00		
50	-83.9	-83.9		-83.9		+0+0	+0+000	+0.000
	-232.9	+416+8	-127.5	-103.4	-2.08	+51.07	+0+000	+0.000

TABLE A-5 (CONCLUDED)

RH%		LHMIN	LREGD	LHMAX	LHRES	LHDSK	LHWSK	WETLR
	SEHET	STØRE	RADHT	CØVSK		PYYHG	CLØSR	CLØDT
AIR	TEMP:	+0.00	SKIN: 31	• 89 C	35. AA MMH	ıc		
0	+25+1	+32+0			+8 • 41		+0+0	+6+0000
	+74.9			+39+2	+4.12	+0.00	+4.116	+27.593
50			-303-1	+30 • 1	+8.01	+15.7	+0.0	+0.0000
100	+76•2 +22•3	+0+0	+32.2	+39+9	+4.21	+2.29		+27-489
.00	+77.7	+0•0	+32.8	+ 40 • 6				+0.0000
AIR		15.00	SKIN: 32	• 11 C	+ 4+ 29 35. RR. MMH	* 4• 38 :G	+3.939	+27.379
0	+29•2	+33+1	-124.2	+33-1	+9.20	+20.0	+0+0	+0.0000
	+70+8	+0•0	+33•4 -124•4	+35.3	+2-14	+0+00	+1.926	+12-528
50	+24.6	+27.5	-124.4	+27.5	+7.90	+16.7	+0.0	+0.0000
100	+75.4 +19.8	+0•0	+35.6	+ 37 • 5	+2.29	+ 6• 39		+12-165
100	+80+2	+21.9 +0.6		+21.9	+ 6 • 59	+13.2		+0.0000
AIR		23.00	SKIN: 32	+39•8 - 40 ° '	+2.45	+12.78	+1+601	+11.789
0	+32+3	+34.0	→27.0	+34.0	nr.m 10•0¢ 23.0+	+22.7	۸۸. ۸	+0 0000
	+61.6	+0.0	-27.0 +33.7	+32.8	+1.08	+0.00		+ 4. 769
50	+23.8	+24.8	-27.2 +38.0	+24.5	+ 7. 42	+16.4		+0.0000
	+ 76 = 1	+0•9	+38.0	+36.8	+1.29	+10.53		+4.103
٥٥ ۳	+12-1	+15.5	- 27 ₄ A	415.5	45.14	+9•9	+0•0	^ O• 0000
ATE	+84.9	+0.0	+ 42. 4	+41+0	+1.51	+21.07	+0.432	+3.413
0	+ 49 - 6	3U+UU	SKIN: 33	• 71 C 3	39.26 MMH			
ŭ	T E V V						+14.2	
50	+49+3	+22-1	+49.3	+308.3	+0.15 +6.62	+14-1	+29.7	+0+000
	+50.7	+0+0	+26.3	+24.0	+0.43	+15.91	+0.000	+0+0931
100	+49.0	+8-1	+ 49 • 0	+99.2	+3-11	+2.7	+ 43 • 2	+0.4499
415	+51+0	+0.0	+26.3 +49.3 +26.3 +49.0 +26.3	-4.0	+0.73	+31.83	+0.000	+0.000
ALR	1011	33400	27141 240	. 30 6 4	11 • 1 / MMH	(5		
0	+ 21 - 1	+37+6	+ 78 • 9	+542.2	+10-24	+25-1		+0.0818
50	+ 78 - 6	+21.0	+11.3 +78.6 +11.3	*1U+1	+0.25	+0.00	+0.000	÷0•000
	+21.4	-0.0	+11.3	÷10.1	+0-13	+11.7	+60.7	
100	+ 46 - 3	T 40 2	+ 18 • 2	+46•3	+1.92	+0.0		+1.0000
	+21.8	+31.9	+11+3	+10-1	+0.41	+37.73		+0.000
AIR	TEMP: +	37.00	SKIN: 35.	30 C 4	2.89 MMH	G		
0	+124+3	+39+0	+124.3	+564.6	+10-48	+23.9	+89+9	+0.1623
50	+123-0	+0+0	-12-5	-11.0	-0.78	+0.00	+0.000	+0.000
30	-23.9	*10.0	+123.9 -12.5 +123.5	+255+4	+5+33	+ 7.1	+111.5	
100	-54-1	-54-1	+123.5	~54.1	*0*40	+23.54	+0.000	
	-23.5	+177.6	-12.5	-11.0	+0.00	+ 47-08		
AIR	TEMP: +	45.00	SKIN: 35.	83 C 4	4.17 MMH	G		. 50000
0	+231+6	+ 40 • 4	+231.6	+581.6	+10.99	+19.0	+201.6	+0-3534
E0.	-131.6	+0•0	-70.6 +231.1	-57.2	-1.85	+0.00	+0.000	+0.000
50	-131-1	+8+5					+106.2	
ALR	TEMP: +	50.00	-70.6 SKIN: 35.	-59.2	-1.32	¢35•95	+0.000	+0.000
0	+303.9	+40.9	+303.9	+586.0	40 40 MMH	+15.3	+277.3	A A A R O E
	-203.9	+0.0	-110.7	~90.7	-2.52	+0.00	+0.000	+0.00C
50	-22-1	-22-1	+303+3	-22.1	+1.06	+0.0	-23.2	
	-203.3	+325•4	-110.7	-90.7	-1.87	+ 46. 28		+0.000
AIR	TEMP? +	50.00	EKIN: 36.	10 C 4	4.81 WWH(
	+ 45c ; 3 - 356+ 3		+ 456+3	+590+9		+ 7. 3	+437.0	
	-336.3 TEMP: +			-154·4		. *0·00	+0•000	+0+000
	+ 593 • 7		SKIN: 36. +617.8	10 U 4	4031 77H(410,71		1501 A	
	-517.8	v24.1		-218-6		+0.0	+581.0	
AIR	TEMP: +8	0.00	SKIN: 36.	20 C 4	5.06 MMH	;		+0•000
0	+ 595• 7	+43• 4	+ 788 • 6	+595.7	+13-47	+0.0	+582+2	1.0000
•	-6 :•6	+192.9	-399 • 1	- 282 • 9	-6.57	+0.00	+0.000	

TABLE A-6
METABOLIC PARAMETERS, SET 5

RHI	LAHET	LAMIN	LREGD	LUMAY	LHRES	LHDSK	Luuer	WETLR
11114	SEHET		RADHT			PMMHG		
	00.10.	J. 0	MADIL.	00151	OBILES	7 1417710	CLUSK	05.001
AIR	TEMP: +	10.00	SKIN: 32	•00 C 3	5.67 MMH	G		
0	+27.5		-251.8	+32+6			+0.0	+0.0000
						+0.00		+18.433
50	+24.4	+28.7	+26.3 -251.9	+43•3 +28•7	+8.02	+16.3		+0.0000
	+75.6	+0.0	+27.5	+45.2	+2.93	+4.60	+2.647	+18+238
100	+21.2	+0.0 +24.7	+27.5 -252.0	+24.7	+7.12	+14-1	+0.0	+0.0000
	+78-8	+0.0		+47.1		+9.20	+2.514	+18.042
AIR		20.00				G		
0	+30.8	+33.6	-100.6	+33.6	+9 • 48	+21.3	+0•0	+0.0000
	+69•2	+0.0	+27.3	+40•4	+1.48	+0.00		+8 • 535
50	+24.0	+25.9	-100.8 +30.0	+25.9	+7.64	+16.4		+0.0000
	+75.9	+0.0	+30+0	+44.3	+1.67	+8.77	+1.152	
100	+17.1	+18.3	-100.9 +32.7	+18.3	+5.80	+11.3	-	+0.0000
	+82.9					+17.53	+1.000	+7.672
			SKIN: 32					
0	+33.0	+34.4		+34.4		+23.2		
	+67.0 +23.3	+0.0	+27.5	+38 • 7	+0.81	+0.00		+3.861
50	+23.3	+24.0	-27·1 +31·5	+24.0	+7.23	+16.0		+0.0000
		+0.0	+31.5	+44.2	+1.05			+3.249
100		+13.5	-27.3	+13+5		+8.6		+0.0000
410	+86.7	+0.0		+49.8	+1.28	+23.76	+0.323	+2.617
			SKIN: 33				40.0	.0.5000
0	+34-1	+35.0	+0•7 +27•4		+9.88	+24•3 +0•00		+0.7000 +2.148
50		+23.2		+23.2		+15.9		+0.0000
30	+77.1	+0.0	+32.1	+ AA - 2	40.80	+13.37		+1.440
100	411.3	+11-4	+0.2	+11.4	+4-10	+7.2		+0.0000
100	+88+6	+0.0	+36.9			+26.74		+0.717
ATR			SKIN: 33				.0.00	
0			+26.3				+0.0	+0.0000
•	~64·5		+27.3		+0.28	+25.5 +0.00		+0.586
50	+26.0	+22.5	425.0		+6.76	+15.6		+0.0082
		+0.0	+31.2	+42.2	+0-56		+0.000	+0.000
100		+9.2	+25.8			+5+1	+17.2	+0-1048
	+74.2	+0.0	+31.2	+42.2	+0.84	+30.04	+0.000	+0.000
			SKIN: 34					
0	+50 • 1	+36.7	+ 50 - 1	+768+3	+10.12	+26.0	+13.9	+0.0184
	+49.9	+0.0	+21.4	+28.5	+C+01	+0.00		+0.000
50	+49.8	+21.8	+49.8	+444.5	+6.46	+14.3	+29.0	+0.0663
	+50.2	-0.0	+21 • 4 +49 • 5	+28.5	+0.31	+16-85		+0.000
100	+49.5	+6.9	+49.5	+120.6	+2.74			+0.3747
	+50.5		421.4			+33.70	+0.000	+0.000
	TEMP: 4	35.00	SK1N: 35	•00 C 4	2.18 MMH	G		
0	+100+5	>38 • 4	+100.5	+811.8	+10.36	+25.8	+64+4	+0.0803
	-0.5	+0.0	-0.0	-0.0	-0.52	+0.00	+0.000	+0.000
50		+19.8	+100+2	+406-5	+5.75	+11+1		+0.2079
			-0.0					
100		+1.0	+99.8	+1.0	+1.02			+1.0000
410	+0.2	+98+8				+42.18	+0:000	+0.000
	TEMP:		SKIN: 35				4141.4	+0.1710
0	+176.3	+39 • 6		+838 • 4		+24.0		
E0	-76.3	-0.0 +15.2	+33+1		-1.19 +4.58	+0.00 +4.7		+0.000
50	+175-8			+306+6		+27.67		+0.000
100	-75.8 -225.4	+0•0 -225•4			-1.74	+0.0		+1.0000
100	-75.4	+400+8	-33-1	-41.9	-0.29	+5:-34	+0.000	
ΔIP		52.00	SKIN: 36					
0	+382.3	+41-1		+858.3		+17.3	+353.4	+0.4175
•	-282.3	+0.0				+0.00		+0.000
50			+381.6	-123.4	+0.12	+0.0		+1.0000
-	-281-6	+504.9	+381.6	-152.0	-2.08	+51.07	+0.000	

TABLE A-6 (CONCLUDED)

RH%	LAHET SEKET		L REOD RADHT				LH WSK CLØSR	WETLR CLØDT
4								
O AIR	TEMP: +25•0		SKIN: 31 -399.9	•89 C 3 +32•0			+ 0.0	+0.0000
Ū	+75.0	+0.0		+45.9	+4.12	+0.00		+28 • 497
50	+23+6	+30+1		+30 • 1	+8 • 01	+15.6		+0.0000
	+ 76. 4	+0.0	+25.5	+46.7	+4.21	+2.29		+28.414
100	+22.2				+ 7. 61		+0.0	+0.0000
4.5	+77.8	+0+0		+ 47.5	+ 4. 29	+ 4• 58	+ 4• 0 68	+28+331
O WIK		15.00	SKIN: 32					
U	+71.0	+0.0	+26.9	+42.0	+9+20	+19-8		+0.0006
50		+27.5		+27.5	+7.90	+16.5		+0.0000
		+0.0		+44.7	+2-29	+6.39		+13-153
100		+21.9	-176.6	+21.9	+6.59	+13-1		+0.0000
	+80.3	+0.0		+ 47 • 4		+12.78	+1.743	+12-858
			2KIN: 35					
0	+32.0	+34.0	-55-5	+34.0		+22.4		+0.0000
50	+67.9	+0.0	P • 1 S +	+39 • 4	+ 1 + US	+0+00		+5.684
30	+ 76 • 3	+24.9	-56.0 -30.8	+ 44.2	+1.29	+10-53		+5.154
100	+15.0	+15-5	- 56- 3	+15.5	+5-16	+9.8		+0.0000
	+85+0	+0.0	+34.4	+49 - 1	¥1.51	+21.07		+ 4 • 605
AIR	TEMP: +	30.00	SKIN: 33	71 C 3				
0	+38 • 4	+36.2		+756-0	+10-06	+26.0	+2.3	+0.0030
	+61·6 +38·1	+0.0		+35-2	+0+15	+0.00		+0•000
50	+38+1	+22-1	+38+1	+ 450 • 2	+ 6 + 62	+14-9	-	+0.0372
100	+37.g	+0+0 +8+1	+26+3 +37+8	+35•2	+0.43	+15.91		+0.000
.00	+62.2	+0•0			+0.73	+3.9 +31.83	+30+8	+0.000
AIR			SKIN: 34	56 C 4	1.17 MMH	G	*0*000	+0•000
U	+ 74. 1	+37.6					+37.8	+0.0484
		-0.0	+11-3	+14.8	-0.25	+0.00		+0.000
50	+73.8	+21.0	+ 73 • 8 + 11 • 3	+ 429 • 9	+6.13	+12-9	+54.8	+0-1292
	+26-2	-0.0	+11+3	+14.8	+0.07			+0+000
100	+67.2 +26.5	+4+2	+73+5 +11+3	+67+2	+1.92	+0.0		+1.0000
AIR		37.00	SKIN: 35	. 7 1 40 B	+0+41	+37•73	+0+000	+0.000
0				+825 • 4			+93.7	+0.1140
	-29.5			-16-1	-0. 'a'	+0.00		+0.000
50	+129.1	+18.2	+129+1	+373.0	+5-33	+8+8		+0.3125
	-29 • 1	+0+0	-12.5	-16-1	-0.40	+23-54		+0.000
100		- 79 • 5						+1.0000
AID	-28.7			-16.1	+0.00	+ 47+ 08	+0•000	+0.000
0	+250.5	43400	SKIN: 35.	4950 I	4 • 1 7 MMH	G +01 A	.007.1	
•	-159.5	+0.0	-70.6		-1.85	+0+00	+227-1	+0.2708
50	+159.2	+0+0 +8+5	+259.0		+3.05	+0.0		+1.0000
	-159.0		- 70 • 6					+0.000
AIR	TEMP: +		SKIN: 35.			G		
0	+346•6	+ 40 • 9	+346+6	+856•5	+11.31	+18+5	+316.8	+0-3748
	-246.6		-110.7		-2.52	+0•00	+0+000	+0.000
50		-33.0		-33.0	+1.06	+0.0		+1.0000
ATD	-246.0 TEMP: +	+379+0	-110+7		-1.87		+0•000	+0.000
0	+528+9		SKIN: 36.	+863•3	4+31 MMH	6 +{2•1	4 50 A. O	+0-5930
•	- 428 • 9		-178.0		-3.87	+0.00	+0.000	+0+000
AIR	TEMP: +		SKIN: 36.				0.000	. 0.000
0	+720.7	+ 42 • 6	+720.7	+867-1	+12.71	+5.3	+ 702 - 7	+0.8224
	-620.7			-321.5		+0.00		+0.000
	TEMP: +		SKIN: 36.					
0	+869.7		+921 • 7			+0+0		+1.0000
	-821.7	+ 32 · U	-399•1	- 416.1	- 6. 57	+0+00	+0.000	+0.000

TABLE A-7
METABOLIC PARAMETERS, SET 6

RH%	LAHET	LHMIN	LREOD	LIMAX	LHRES	LHDSK	I.HWSK	WETLR
	SEHET	STORE	RADHT					
AIR	TEMPs +	10.00	SKIN: 32	00 C 35	5.67 MMH	3		
Q	+27 . 3	+32.6	-335-4	+32.6	+8.93	+18.4	+0.0	+0.0000
	+72.6	+0.0	+21.1	+48.8	+2.80	+0.00	+2.894	+19.157
50	+24.2		-335-5		+8.02	+16.2	+0.0	+0.0000
	+75.8	+0.0	+22.0		+2.93	+4-60	+2.753	+19.003
100	+21.1		-335-6		+7.12	+13.9	+0.0	+0.0000
•••	+78.9	+6.0	+22.9	+52.9		+9.20		+18.846
AIR		20:00	SK IN: 32					
0	+30.6	⇒33•6		+33./			+0.0	+0.0000
•	+69.4			+45.9	+1 - 48	+0.00	+1.441	+9.278
50	+23.9	+25.9		+25.9		+16.2		+0.0000
30	+76.1		+24.2			+8.77		+8.938
100	+17.0	≯18∙3		+18.3			-	+0.0000
100		+0+0		♦54.7	+1.86	+17.53		+8.591
ATO	+83.0		SKIN: 32				*******	.00371
	TEMP: +			+34•4			A0.0	+0.0000
0	+32.8	+34.4						+4.607
	+67.2		+22.3	+44-1		+0.00		+0.0000
50	+23 • 1		-56.4 +25.5	.54.0	+7.23			+4.120
	+76.9	+0+1	+25.5	+50+3	+1.05			
100	+13.2	+13.5		+13.5		+8+5		+0.0000
	+86.8					+23.76	+0.446	+3.617
			SKIN: 33	00 C 3	7.73 MMH	G		
0	+33.9	+35%0		+35.0	+9.88	+24.0		+0.0000
	+66-1	+0.0	+22.3	+43.3	+0.55	+0.00		+2.892
50	+22.7	+23.2	-22.3 +26.1	+23•2	+7.01	+15.7		+0.0000
	+77+3	^9•0	+26.1					+2.328
100	+11.3	+11-4	-22.6		+4.10			+0.0000
	+88.7	+0.0	+29.9				+0.210	+1.748
AIR	TEMP: +	25.00	SKIN: 33	• 44 C 31	B.67 MMH	G		
0	+35.2	+35.7	+9+5	+35.7	+10.00	+25.2	+0•0	+0.0000
	+64.8	+0.0	+22•2 +9•2	+42.3	+0.28	+0.00	+0.217	+1.326
50	+22.3	+22.5	+9•2	+22.5	+ 8.76	+15•6	+0+0	+0.0000
	+77.7	+0.0	+26.6	+50+5	+0.56	+15.02	+0.093	+0•678
100	+9.2	+9.2	+8.9	+9.2	+3.46	+5•7	+0.0	+0.0000
	+90.8	+0.0	+31 • 1	+58+8		+30.04	+0.005	+0.017
AIR	TEMPs +	31.00	SKIN: 34	•00 C 3	9.90 MMH	G		
0	+38.7	+36.7	+38.7	+1071.6	+10.12	+26.5	+2.1	+0.0020
	+61.3		+21.4	+39.9	+0.01	+26.5 +0.00	+0.000	+0.000
50	+38.4	+21.8	+38.4	+619.7	+6.46	+14.9		+0.0276
	+61.6	+0.0	+21.4	+39.9	+0.31	+16.85	+0.000	+0.000
100	+38-1	+6.9	+38-1		+2.14		+32.0	+0.1941
	+61+9	-0.0	+21.4		+0 62	+33.70	+0.000	+0.000
AIR			SKIN: 35			G		
	+100.5		+100-5				+63.7	+0.0568
		+0.0	-0.0	-0.0	-0.52	+0.00	+0.000	
50	+100+2	+19.8	+100.2	-0.0 +566.8	+5.75	+12.0	+82.4	+0.1470
-	-0.2	-0.0	-0.0	-0.0	-0.16	+21.09	+0+000	
100	+1.0	+1.0	+99.8	+1.0	+1.02	+0+0		+1.0000
.00	+0.2	+98-3	-0.6	-0.0	+0-20	+42.18	+0.000	
AIR	TEMP: +		SKIN: 35		3.56 MMH		41000	
ō	+193.0	+39.6	+193.0		+10.67	+25.0	+157-3	+0.1358
U	-93.0	•0•0	-33.1	-58.7	-1.19	+0.00	+0.000	
40				+427.4	+4.58	+6+0		+0.4304
50	+192.6	+15.2	+192.6	-58.7	-0.75	+27.67	+0<000	
100		+0.0 -214.9			-1.74	+0.0		+1.0000
100	-314.9	-314.9	+192.1	-314.9			+0.000	
	-92-1	+507 • 1	+33+1	-58.7	-0.29	+55•34	+0•000	+0+000
	TEMP: +		SKIN: 36				4410 0	AO - 2 AT F
0	+443 • 1	+41+1		+1197.0	+11.45	+19.3		+0.3478
	-343-1	-0.0		-212-8	-2.79	+0+00	+0.000	
50	-172.8	-172.8		-172-8	+0.12	+0+0		+1.0000
	-342.4	+615-1	-127.5	-212.8	-2.08	+51+07	+0.000	+0.000

TABLE A-7 (CONCLUDED)

RH#	LAHET SEHET	LHMIN STØRS	LREOD RADHT	LHMAX CØN SK	LHRES CORES	LHDSX PMMHG	LHWSK CLØSR	WETLR CLØDT
	=0404	+0-00	SKIN: 31.	89 C 3	5.44 MMH	;		
	•		-521.1	+ 32 • 0	+8.41	+16-4		0.0000
0	+24·8 +75·1	+0.1	+19.8	+51+1	+4.12	+0.00	+ 4.340 +	
60	+23.5	+30+1			+8.01	+15.5		0.0000
50	+76.4	+0.1	₹20•2		+ 4.21	+2.29	+ 4. 254 4	
100	+82.1	+28 • 1		+28 - 1	+ 7. 61	+14.5		0.0000
100	+77.9	+0.0	+20.6	+53.0	+ 4. 29		+4.169 4	29.076
ATO	TEMP: +		SKIN: 32	11 C 3	5.88 MMH	3		
0	+28 • 8		-241.2	+33-1	+9 • 20	+19+6		0.0000
· ·	+71.2		+21.6	+ 47. 4	+2-14	+0.00	~2.167	
50	+24.2	_	-241.4		+ 7• 90	+16.3		0.0000
•	+75.7	+0+1	+23.0	+50 • 4	+2.29		+2.004	
100	+19.5		-241.6	+21.9	+ 6• 59	+13.0		+0.0000
•••	+80.4	+0.0	+24.5	+53.5			+1-855	13.712
AIR	TEMP:	23.00	SKIN: 32	• 49 C 🤅	36.67 MMH	G		
0	+31+8	+34+0	-91.9	+34.0		+ 22 • 1		+0.0000
	+68 • 2	+0.0	+55.5	+ 44.9	+ 1 • 08 + 7 • 42 + 1 • 29	+0.00	+1.011	
50	+23+4		-92.1	+24.8	+ 7. 42	+16.0		+0.0000
	+76+5	+0.0	+ 25• 0			+10.53	+0.842	
100	+14.9	+15.5	-92.3	+15.5		÷9•7	+0.703	+0+0000
	+35•1	+0•0	+27.8	+55+8	+1.51	+21.07	+0+ /03	+3+371
AIR	TEMP:	+30+00		•71 C	39.26 MMH	ŭ . 05 0	+0.0	+0.0000
0	+35.9				+10.06	+25.9		+0•600
	+64-1		+ 55 • 5	+41.7		+ 0 • 00 + 15 • 5		+0.0030
50	+24.0	+22.1	+24.0	+627.7		-		+0,000
	+76•0			+ 49 • 3		+15.91	+16.0	+0.0810
100	+23.7		+23•7	+200-9		+31.83	+0.000	+0+000
	+ 76 • 3	+0+0	+26+3	+ 49 • 3	+0.73		.0.000	. 00 000
				1. 56 U	41 - 1 7 MMH	+26.6	+31.4	+0.0286
0	+68.2		_		+10-24	+0.00		+0.000
	+31+8		+11-3	+20+8		+13.6		+0.0811
50	+67•9			+599•4 +20•8				+0.000
	+32+1	_		+93.4		+0.7		+0.7104
100	+67.5		_			+37.73	+0.000	+0+000
A	+32.5			. 30 C	42.89 MMH			
		+37.00 +39.0		+1151.4	+10-48	+26.0	+99.4	+0.0871
U	+135.9			-22-6		+0.00	+0+000	+0.000
50	-35·9 +135·5					+9.9		* 0 · 2338
50	-35-5					+23.54	40.000	+0.000
100	-111+3					+0+0	-111.3	+1.0000
100	-35.1					+ 47• 08	+0.000	+0•000
ΔΤΕ	TEMPS	+45.00	SKIN: 35	5.83 C	44.17 MMH	IG		
0	+294.3	+40 • 4	+294.3	+1185.8	+10.99	+ 22 • 9		+0+2217
•	-194.3		-70.6	-121.9	-1.85	+0•00	+0.000	+0.000
50	+221 • 6		+293.8	+221 • 6	+3.05	+0•0	+218.6	+1.0000
•	-193-8		- 70 • 6	-121.9	-1.32	+35.95	+0•000	+0.000
AIF	R TEMP:	+50.00	SKIN: 35	5.96 C	44. 48 MM	1C		
0			+399.9	+1194-6	+11+31	+20 • 4		+0.3112
•	-299 • 9		-110-7	186.7	-2.52	+0.00	+0+000	
50	- 46.		+399+3		7 +1.06	+0+0		+1.0000
	-299 • 3		-110.7	-186-1	7 -1.87	+ 46 • 28	+0+000	+0+000
AII	R TEMP:	+60.00	SKIV: 3	6•10 C	44.81 MM	16		. 0 4074
0			+619.5	+1203+8	+12.00	+15.0		+0-4974
	-519 • 8	-0.0	-198-0	-317-9	-3-87		÷0•000	+0.000
AII	R TEAP:	+70.00	SKIN: 3	6.16 C	44.97 MM	16	A 0 0 7 . A	+0-6917
0		3 +42.6	6 +849+3	+1208 • 9	+12.71	+9.2		
	-749 -		-294.0	- 450 • (-5.21	+0+00	+0+000	+ 0 + 0 0 0
AI	R TEMP:	+80+00	SKIN: 3	6.20 C	43.06 MM	אל א אול א	A1071.5	+0.8939
	+1088+	2 +43•	4 +1088 2				+0.000	+0.000
	-988	S +0•(- 399•1	-582•	5 -6.57	+0.00	+04000	

TABLE A-8
METABOLIC PARAMETERS, SET 7

RHX	LAHE	T LHMIN	LREOD	LHMAX	LHRES	Lunev	LHWSK	
	SEHE	T STØRE	RADHT	CONSK				
							CLØSR	CLODT
ΑI	R TEMP:	+10.00	SKIN: 3	2 00 0	25 45			
	171.	7 +0 0	+0.0 +0.0 -70.1 +0.0 -70.3	+32+6	+8.93	+19.4	+0+0	+0.0000
50	425	1 400	+0.0	+ 68 • 9	+5.80	+0.00	+2.236	+14.594
-	174	720.1	-70.1	+28.7	+8.02	+17.1	+0.0	+0.0000
100	1740	+0.0	+0.0	+71.9	+2.93	+4.60	+2.078	+14-164
100	+21.	+24.7	-70.3	+24.7	+7.12	+14.8	+0-0	+0 0000
	+78•	+0.0	+0.0	+75.1	+3.05	+9.20	+1.929	+12 701
AH	R TEMP:	+50.00				10	*10727	+13.721
0	+32.	1 +33.6	+5.1 +0.0 -4.9 +0.0 +4.7 +0.0 SKIN: 32	+33.6	49.48	***		
	+67.9	+0.0	+0.0	+66.4	41 40	T22.6	+0.0	+0.0000
50	+25.2	+25.9	44.9	+25.0	¥ 1 • 40	+0.00	+0 • 650	+4.091
	+74.8	3 +0-0	10.0	120.0	+ /+ 64	+17.5	+0•0	+0.0000
100	+17.0	118 2	10.0	+/3.2	+1.67	+8.77	+0.443	+3.074
	489.0	710.3	+4.7	+18.3	+5.80	+12.1	+0.0	+0.0000
ATO	TEND	, , , , , , ,	+0.0	+80.2	+1.86	+17.53	+0.265	+2.015
411	LEMPI	+25.00	SKIN: 32	2.70 C	37.10 MMH	IG		
0	+40.7	+34.4	+40.7 +0.0 +40.4 +0.0 +40.2 +0.0	+573.7	+9.76	+24.4	44.5	40.0117
	+59.3	-0.0	+0+0	+58.5	+0.81	+0-00	+0.000	+0.0116
50	+40.4	+24.0	+40.4	+390+6	+7.23	+160	+0.000	*0.000
	+59 • 6	+0.0	+0.0	458.5	11.00	T10.0	+17.2	+0.0449
100	+40.2	+13.5	+40.9	+007 5	+1.05	+11.88	+0.000	+0.000
	+59.8	-/-0	+0.0	7207.5	+4+67	+7.7	+27.9	+0.1375
AIR	TEMP	427 00	CV 1 N + 00	+58.5	+1.28	+23.76	+0.000	+0.000
0	452.0	127400	SKIN: 33	•00 C 3	7.73 MMH			
•	+ 33 • 9	+35.0	+53.9	+583•4	+9.88	+24.2	+19.7	+4.0344
	T 46+ I	-0.0	+0.0	+45.6	+0.55	-0.00	+0.000	+6.000
50	+53+6	+23.2	+53.9 +0.0 +53.6 +0.0 +53.3	+377.3	+7.01	+14.8	+31.8	+0 0000
	+46•4	+0.0	+G.O	+45.6	.0.80	+13.37	40.000	+0.000
100	+53.3	+11.4	+53.3	+171.2	+4-10	45.4	+43.8	+0.000
	+46.7	+0.0	+53+3	+45.6			+43.8	+0.2624
AIR	TEMD.	420 00	CIVINIA DO		_	720.14	+0.000	+0.000
0	+66.0	+35.7	144 0	• ~ 4 6 3	2.6/ WWH	6		
_	+34.0	-0.0	+66.0 +0.0 +65.7 +0.0 +65.4 +0.0	+397.8	+10.00	+24.3	+31.7	+0.0539
52	445 7	100.5	+0.0	+33.7	+0.28	+0•00	+0.000	+0.000
J.	+03•1	+22.5	+65+7	+366.2	+6.76	+13.7	+45.2	+0.1258
100	+34.3	-0.0	+0+0	+33.7	+0.56	+15.02	+0.000	+0.000
100	+65.4	+9.2	+65~4	+134.6	+3.46	+3.2	+58.8	10 0000
	+34.6	+0.0	+0,0	+33.7	+0.84	+30.04	±0.000	10 000
AIR	TEMP: .	+31.00					+0.000	+0.000
0	+77.2	+36.7	+77.2 +0.0 +76.9 +0.0 +76.5 +0.0 SKIN: 35.	+616.7	*10 10	, , , , ,		
	+22.8	+0.0	±0.0	100.0	10.12	+24.1	+48 • 4	10.0699
50	+76.9	+21.9	176.0	1254.0	+0+01	+0.00	+0.000	+0.000
	423.1	. 21.0	7 (0.9	+356.9	+6+45	+12.8	+57.6	0.1644
100	474 4	+0.0	\$U.U	+55.8	+0.31	+16.85	+0.000	+0.000
100	¥ / 6 • 6	+6+9	+76+5	+97.1	+2.74	+0.9	+72.9	0.7730
4.5	+23.4	+0.0	+0.0	+22.8	+0 • 62	+33.70	+0.000	+0.000
AIR	EMP: 4	35.00	SKIN: 35.	00 C 42	2.18 MMHG	;		
0	+100.5	+38.4	+100.5 +0.0 +100.2 +0.0	+651.5	+10.36	+25.2	445.0	0 1010
	-0.5	+0.0	+0.0	-0.0	-0.52	10.00	10000	0.1013
50	+100.2	+19.8	+100.2	+396.3	A 5 . 7 E	410	+0.000	+0.000
	-0.2	-0.0	+0.0	-0.0	73473	+10.3	+84-1 +	0.2622
100	+1.0	+1.0	+99.8	-010	-0.10	+51.03	+0.000	+0.000
	+0.2	+98+8		+1.0	+1.02	+0.0	~0.Q +	1.0000
ΔΙΟ	TEMP: +		+0.0	-0.0	+0.20	+42.18	+0.000	+0.000
	15000		SKIN: 35.	58 C 43	3.56 MMHG			
0	+134.7	+39.6	+134.7	+672.9	+10-67	+24.6	99.5 +	0.1502
	-34.7	+0.0	+0.0	-33.6	-1.19			+0.000
50	+134.3	+15.2	+134.3	+246.2	+4.58		+124.6 +	
	-34.3	+0.0	+0.0	-33.6	-0.75		.18446 4	
100	-180.7	-180.7		-180.7			+0.000	+0.000
	-33.8	+314.5	+0.0		-1.74		-178.9 +	1.0000
AIR	TEMP: +			.33.6	-0.29	+53.34	+0.000	+0+000
	+224.4		KIN: 36.		• 57 MMHG			
		+41 - 1			+11.45	+21.3	+191.7 +	0.2830
	-124.4	+0.0		121.6	-2.79			+9.600
50	-98.7	-98.7	+223.7	-98.7	40.12	+0.0	-98.8 +	1.0000
	-123.7	+322.4	+0.0	-121.6				
							. 5 - 6 0 0	+0.000

```
LREQD
                                       LHRES
                                               LHDSK
                                                       L4 WSK
                                                                WETLR
              LHMIN
                              LHMAX
RH%
     LAHET
                                                       CLØSR
                                                               CLØDT
                                       CARES
                                               PMMH G
              STORE
                      RADHT
                               CANSK
      TEKET
                    SKIN: 31-89 C 35-44 MMHG
AIR TEMP: +0.00
                                                        +0.0 +0.0000
                                               +17.1
     +25.5
              +32.0
                     -146.5
                              +32.0
                                       +8.41
 Ú
               +0.0
                       +0.0
                              +70.3
                                       +4.12
                                               +0.00
                                                      +3.776 +25.171
      + 74. 4
                                       *8.01
                                               +16.1
                                                        +0.0 +0.0000
                              +30.1
 50
      +24.1
              +30.1
                     -146.6
                                               +2.23
                                                      +3-682 +24-997
      + 75.9
               +0.0
                       +0.0
                              +71.6
                                       + 4.21
                                       +7.61
                                               +15.1
                                                       +0.0 +0.0000
              +28-1
                     -146.6
                              +28 - 1
100
      +22.7
                                      + 4. 29
                                               + 4. 58
                                                      +3.589 +24.821
                      +0.0
                              +73.0
      +77.3
               +0.0
 AIR TEMP: +15.00
                    SKIN: 32-11 C 35-88 MMHG
                                       +9.20
                                               +20.8
                                                        +0.0 +0.0000
              +33-1
                      - 32 - 1
                              +33+1
      +30.0
  Λ
                                               +0.00
                                                      +1.449 +9.311
                                       +2.14
      +70.0
               +0.0
                       +0.0
                              +67.8
                                                        +0.0 +0.0000
              +27.5
                      -32.3
                              +27.5
                                       + 7. 90
                                               +17.4
 50
      +25.3
                                               +6.39
                                                      +1.261 +8.647
              +0.0
                       +0.0
                              +72.4
                                       +2.29
      +74.7
                                               +13.8
                                                        +0.0 +0.0000
                                       +6. 59
100
      +20.4
              +21.9
                      -32.5
                              +21.9
                                                      +1.089 +7.958
      +79.5
               +0.0
                       +0.0
                              +77-1
                                      +2.45 +12.78
                   SKIN: 32.49 C 36.67 MMHG
 AIR TEMP: +23.00
                                               +24.0
                                                        +0.0 +0.0000
      +33.6
              +34.0
                      +26.8
                              +34.0
                                      +9.65
                               +65.3
                                       +1.08
                                               +0.00
                                                      +0-169 +1-045
               +0.0
                       +0.0
      +66.4
                             + 404.7
                                       + 7. 42
                                               +17.3
                                                        +1.8 +0.0046
                      +26.6
 Sn
      +25.6
              -24.8
                                      +1.29
                                              +10.53
                                                      +0.000 +0.000
               +0.0
                       +0.0
                              +72.1
      + 73. 4
                                       +5.16
                                                +9.9
                                                       +11.3 +0.0476
                      +26.3
                             +242+4
              +15.5
100
      +26.3
                              + 72 - 1
                                              +21.07
                                                      +0.000 +0.000
                                      +1.51
      +73.7
               -0.0
                       +0.0
 AIR TEMP: +30.00
                    SKIN: 33.71 C 39.26 MMHG
                                               +24.5
                                                        +37-1 +0-0622
              +36.2
                      +71.7 +606.8 +10.06
 ٥
      +71.7
                                               +0.00
                                                      +0.000 +0.000
                              +28.2
                                      +0.15
      +28 - 3
               -0.0
                       +0.0
                                                       +51.5 +0.1451
                      +71 . 4
                             +361 • 5
                                       +6.62
                                               +13.3
 50
      +71.4
              +22.1
                                                      +0.000 +0.000
                              +28.2
                                       +0.43
                                             +15.91
      +28.6
               +0.0
                       +0.0
                                       +3-11
                                                +2.1
                                                       +65.9 +0.5833
100
      e 71 · 1
               +8.1
                      +71 - 1
                             +116.1
                              +28 • 2
                                       +0.73
                                             +31.83
                                                      +0.000 +0.000
      +28.9
               +0.0
                       +0.0
                    SKIN: 34-56 C 41-17 MMHG
 AIR TEMP: +33.00
                                               +25.1
                                                       +53-1 +0-0848
                      +88.4 +636.0 +10.24
              +37.6
      +88 • 4
      +11.6
               -0.0
                       +0.0
                              +11.9
                                      -0.25
                                               +0.00
                                                      +0.000 +0.000
                                                        +70.2 +0.2070
                       +88.1 +345.1
                                       +6.13
                                               +11.8
              +21.0
 50
      +88 - 1
                                              +18.87
                                                      +0.000 +0.000
               -0.0
                       +0.0
                              +11.9
                                       +0.07
      +11.9
                                       +1.92
                                                +0.0
                                                       +52.2 +1.00C0
100
      + 54, 2
               +4.2
                      +87.7
                              +54.2
                                       +0.41
                                              +37-73
                                                      +0.000 >0.000
                              +11.9
      +12.3
              +33.5
                       +0.0
 AIR TEMP: +37.00
                    SKIN: 35.30 C 42.89 MMHG
                                               +25.1
                                                        +78 - 1 +0 - 1198
     +113.7
              +39.0
                     +113.7 +662.4 >10.48
                                               +0.00
                                                      +0.000 +0.000
                                       -0.78
      -13.7
               +0.0
                       +0.0
                             -12.9
                                                        +99.5 +0.3381
                     +113.3 +299.5
                                       +5.33
                                                +8.5
 50
     +113.3
              +18.2
                              -12.9
                                       ~0.40
                                              +23.54
                                                       +0.000 +0.000
               +0.0
                       +0.0
      -13.3
                                       +0.00
                                                        -63.6 +1.0000
                                                +0.0
              +63.6
                     +112.9
                              -63.6
100
      -63.6
                              -12.9
      -12.9 +176.5
                       +0.0
                                       +0.00
                                              +47.08
                                                       +0.000 +0.000
                    SKIN: 35-83 C 44-17 MMHG
 AIR TEMP: +45.00
                    +171.5 +682.3 +10.99
                                               +23.4 +137.2 +0.2043
              + 4G • 4
     +171.5
                              -69.7
                                       -1.85
                                               +0.00
                                                     +0.000 +0.000
               +0.0
                       +0+0
      - 71 - 5
                     +171.0 +127.9
                                       +3.05
                                                +0.0
                                                      +124.9 +1.0000
     +127.9
               +8.5
                                                       +0.000 +0.000
                                             +35.95
      -71.0
              +43.9
                       +0.0
                              - 69 • 7
                                      -1.32
 AIR TEMP: +50+00
                    SKIN: 35.96 C 44.48 MMHG
                     +209.2 +687.4 +11.31
+0.0 -106.7 -2.52
                                               +21.9
                                                      +176.0 +0.2603
             ÷ 40 • 9
  0 +203.5
                                               +0.00
                                                       +0.000 +0.000
     -109.2
               +0.0
                       208.5 -26.2 +1.06 +0.0
+0.0 -106.7 -1.87 +46.28
                                                       -27.3 +1.0000
                     +208 • 5
 50
     -26.2
              -26.2
                                                       +0.000 +0.000
     -108.5 +234.8
 AIR TEMP: +60.00
                    SKIN: 36-10 C 44-81 MMHG
                    +285.5 +693.0 +12.00
+0.0 -181.7 -3.87
                                              +18.6 +254.9 +0.3743
              +41.8
    +285.5
                                               +0.00 +0.000 +0.000
     -185.5
               -0.0
 AIR TEMP: +70.00 SKIN: 36.16 C 44.97 MMHG
              +42.6 +362.4 +696.2 +12.71
-0.0 +0.0 -257.2 -5.21
                                                +15.3 +334.4 *0.4892
    +362.4
                                                +0.00
                                                      +0.000 +0.000
     -262.4
 AIR TEMP: +80.00 SKIN: 36.20 C 45.06 MMHG
             +43.4 +439.4 +698.5 +13.47
                                               +11.9 *414-1 +0.6046
  C +439 · 4
                        +0.0 -332.9
                                      - 6. 57
                                               +0.00 +0.000 +0.000
               +0.0
     -339.4
```

TABLE A-9
METABOLIC PARAMETERS, 3ET 8

RHI	LAHET			LHMAX	LHRES	LHDSK	LHWSK	WETLR CLØDT
	SEHEI	SINKE	RADHT	CONSK	CORES	PMMHG	CLUSK	CLODI
			SKIN: 32					
0	+27 • 8	+32•6	-143.9	+32.6	+8.93	+18.9	+0.0	+0.0000
50	472.2 404.7	+0+0	+19.4 -144.0 +20.3	+50.0	+2.80	+9.00	+2.551	+16.763
30	+75.3	+20•1 +0.0	-144.0	+28+1	+8.02	+16+7	+0+0	+0.0000
100	+21.5	+24.7	-144-2	±21.7	47.19	+14.4	+0.0	+0.0000
	+78.5	+0.0	+21.2	+54.3	+3.05	-9.20		+16.175
AIR			SKIN: 32	.29 C 3	6.26 MMH			
0	+31.3	+33.6	-37.3	+33.6	+9.48	+21.8	+0.0	+0.0000
	+68.7	+0•0	+20.3	+46.9	+1 • 48	+0.00	+1.053	+6.705
50	+24.5	+25.9	-37.5	+25.9	+7 • 64	+16.8	+0+0	+0.0000
	+/5.5	+0.0 +18.3	+22.3	+51.5	+1.67	*8.77	+0.866	+6.058
100	+82.5	+15.3		+18.3				+0.0000
AIR			SKIN: 32	.70 C 3	71000 7.10 MMH	+ 17 • 33	+0.705	+3.36/
0	+33.7	+34.4	+13.7	+34.4	+9.7.	+23.9	+0.0	+0.0000
	+66.3	+0.0	+20.5 +10.5 +23.6	+45.0	+0.81	+0.00		+1.954
50	+23.8	+24.9	+10.5	+24.0	+7.23	+16.5	+0.0	+0.0000
	+76.2	+0•0	+23.6	+51.6	+1.05	+11.88		+1.009
100	+13.5	+13.5	+:3.2	+13.5	+4.67	+8•9		+0.0000
ATD			+26.9				+0.004	+0.032
0			SKIN: 33 +32.7				40.0	+0.0000
Ū	+65.1	+0.0	+20.4	+44.1	+0.55	+0.00	+0.036	+0.0000
50	+32.4	+0.0 +23.2	+32.4	+377.3	+7.01	+15.8		+0.0260
	+67+6	+0.0	+21.2	+ 45 • 6	+0•80	+13.37		+0.000
100	+32.2	+11.4	+32.2	+171.2	+4.10	+6.4	+21.7	+0.1299
	+67.8			+45.6			+0.000	+0.000
AIR	TEMP: +	29.00	SKIN: 33	• 44 C 3	8.67 MMH	G		
Ü	+50.2	+35•7	+50+2	+597.8	+10.00	+25.1	+15+2	+0.0258
50	+ AQ . Q	+22.5	+15•8 +49•9	+366.9	+4.74	+14-5	+0.000	+0.0798
50	+50 - 1	-0.0	+15.8	+33.7	+0.56	+15.02		+0.000
100	+49 • 6	+9.2	+15.8 +49.6	+134.6	+3.46	+3.9		+0.3226
	+50 • 4	-0.0	+15.8	+33.7	+0.84	+30+04	+0.000	+0.000
			SKIN: 34			G		
0	+66•4	+36.7	+66.4	+616.7		+25.2		
50	+33+6	-0.0 +21.8	+10+8	+22+8	+0.01	+0.00	+0.000	+0.000
50	+33.9	+0.0	+66•1 +10•8	+336+9 +30. g	₹0+46 ±0.31	+13.3	+46+3 +0.000	+0.1323
100	+65.8	+6.9	+65.8	+97.1	+2.74	+1.4	+61.6	+0.6536
	+34.2	+0.0	+10.8	+22.8	+0.62			+0.000
AIR	TEMP: +	35.00	SKIN: 35	•00 C 4	2.18 MMH	G		
0	+100-5	+38.4	+100.5	+651.5	+10.36	+25.2	+65•0	+0.1013
	-0.5		-0.0					
50			+100.2					+0.2622
100	-0.2	-0.0	+99•8	-0.0	-0.16	+21.09	+0.000	+0.000
100	+1.0	+1.0 +98.8	-0.0	+1.0	+1.02	+42.18	+4.000	+0.000
ATR	TEMP: +		SKIN: 35		3.56 MMH		. 3.000	
0	+151-1	+39.6	+151.1	+672.9	+10-67	+23.9	+116.6	+C.1761
	-51.1	-0.0	-16.4	-33.6	-1.19	+0.00	+0.000	+0.000
50	+150.7	+15.2	+150.7	+246+2	+4.58	+4.4		+0.5866
	- 50 - 7	+0.0	-16.4	-33.6	-0.75	+27.67	+0.000	+0.000
100	-180.7	-180.7	+150.2	-180.7	-1.74	+0.0		+1.0000
AID	-50.2	+330+9	-16.4 SKIN: 34	-33.6	-0.29 4.57 MMH	+55.34	+0.000	+0.000
O WIK	TEMP: +	\$41.1	\$KIN: 36 +285.7	+688+9	4.57 MMH +11.45	+18.4	+255.8	+0.3776
J	-185.7	+0.0	-61.3	-121.6	-2.79	+0.00	+0.000	+0.000
50	-98.7	-98.7	+285.0	-98.7	+0.12	+0+0		+1.0000
	-185.0	+383.7	-61.3	-121-6	-8.08	+51.07	+0.000	+0.000

RH \$	LAHET SEHET		LREQD RADHT	LHMAX CƏNSK	LHRES CØRES		lh wsk Closr	WETLF CLØD1
AI	R TEMP:	+ 1× 00	SKIN: 31		25 44 MM			
0	+25.2	+32.0	-250-9	*07 C ,	33•44 MMH	16		
•	+74.8	+0.0	+1g-3	+52.4	+4.12	+16+8		+0.0000
50		+30-1	-251-0	+30-1	44.12	+0.00	+4.029	+26.975
	+76.2	+0.0	-251 • 0 +18 • 6	+ 50 · 1	+8.01	+15-8	+0.0	+0.0000
100			-251.0	4 28 - 1	+ 7. 61	+2.29		+26.852
	+77.5		+18.9	+54-3	+ 4. 29			+0.0000
AI	R TEMP:	+15.00	SK IN: 32	•11 G	35.88 MMU	+ 4• 58	+3-851	+26.731
0	+29.4	+33-1	-90-4	+33.1	49.20	+20.2		
	+ 70 • 6	+0.0	+19.9	+48.5	+2.14	AD. 00	*U•U	+0.0000
50	+24.8	+27.5	+19.9 -90.5	+27.5	+7.90	+16-9	* 1 • 6 U 4	+11+696
	7 13.2	+0.0	+21.2	+51.7	+2.29	+6-39	+1-629	+0.0000
100	+20.0	+21.9	+21·2 -90·7	+21.9	+6.59	+13.4	+0.0	+0.0000
	+80+0	+0•0	+22•6	+54.9	+2.45	+12.7R		+10.808
AIS	R TEMP:	23.00	SKI:1: 32	. 49 C 1	4. 47 MMU	C		
0	+32.6	+34.0	-6.3 +20.4 -6.5	+34.0	+9 • 65	+23+0	+0.0	+0.0000
	+ 67• 3	+0•0	+20•4	+ 45•8	+1.08	+0.00	+0.606	+3-805
50	+24-1	+24.8	-6.5 +23.1 -6.7	+24.8	+7.42	+16.7	+0.0	+0.0000
	+ 75 • 9	+0•0	+23-1	+51.5	+1 - 29	+10-53	+0.423	+2.989
100	+15.3	+15.5	-6.7 +25.8	+15.5	+5.15	+10-1	+0.0	+0.0000
	TO 40 /	+0.0	+25.8	+57.3	+1.51	491.07	+0-272	+2.148
AIN	TEMP:	30.00	SKIN: 33:	71 C 3	9.26 MMH	C		
0	+ 58 • 4	+36.2	+58 • 4	+606+8	+10+06	+25.1	#23·3	+0.0390
	+41.6	+0+0	+13.3	+28 • 2	+0.15	+0+00	+0.000	+0.000
50	+ 58 • 1	+22•1	+13.3 +58.1 +13.3 +57.8 +13.3	+361.5	+ 6- 68	+13.9	+37.6	>0.1060
100	+41.9	+0+0	+13+3	+28 • 2	+0.43	+15.91	+0.000	+0.000
100	+ 40 0	+8+1	+57.8 +13.3	+116.1	+3.11	+2.7	+ 52 • 1	+0.4606
ATD							+0.000	+0.000
0	499.7	133.00	SKINE 34.	56 C 4	1-17 MMH	G		
U	+17.3	+3/·6	+82.7	+636.0	+10-24	+25.3	+ 47•2	+0.0754
50	+R2. A	421.0	+5.7 +82.4 +5.7 +82.1	+11.9	-0.25	+0.00	+0.000	+0.000
-	+17.6	*21•0	702+4	+345-1	+6.13	+12.0	+64.2	+0.1895
100	+54.2	-0.0	+30 /	+11.9	+0+07	+18.87	+0•000	+0.000
	+17.9	+27.0	+5.7	+54.2	+1.92	+0.0	+ 52 • 2	+1.0000
AIR		37.00	SYIN: 35.	711.9	+ 0 • 41	+ 37• 73	+0.000	+0.000
0	+119.9	+39.0	4110.0	30 C 4	2	š		
	-19.9	+0+0	+119.9	-12.0	-0.70	+24.8	+84.6	+0.1298
50	+119.6	+18.2	*119.6 -6.2	+ 200. S	- U+ 78	+0.00	+0.000	+0.000
	-19.6	+0.0	-6.2	-12.0	=0.40	10.54		+0.3603
100	-63.6	-63.6	+119+2	-63.6	+0.00			+0.000
	-19.2	+185.8	-6.2	-12.9	+0.00	+ A7. 00	-63.6 +0.000	* 1 • 0000
AIR	TEMP: +	45+00	SKIN: 35.	83 C A	A. 17 MMU	•		
O	+206.0	+ 40 • 4	+206•0 -34•5 +205•5	+682.3	+10.99	+21.R	+173.2	+0.2501
	-106.0	+0.0	-34.5	- 69 • 7	-1.85	+0.00	+0-000	+0-000
50	+127.9	+8.5	+205.5	+127.9	+3.05	+0.0	+124.9	+1.0000
	-102+2	+77+6	-34.5	- 69 • 7	-1:32	+35-95	+0.000	+0.000
	TEMP: +	50•00	SKIN: 35.	96 C 44	48 MMH 6	3	0.000	. 00 000
0	+262.7	+ 40 • 9	+262.7	+ 68 7 • 4	+11.31	+19+4	+232.0	+0.3431
	-162.7	+0•0	- 53• 5	-106.7	-2.52	+0.00	+0.000	+0.000
30	-26.2	-26.2		- 26. 2	+1.06	+0.0	-27.3	+1.0000
4	-162-1	+288 • 3	- 53• 5	-106.7	-1.87	+ 46. 28	+0.000	+0.000
	TEMP: +		SKIN: 36.		•81 MMHG	-		
0	+379+0		and the same of th	693.0	+12.00		+352.6	+0-5178
A+ D	-279.0	+0.0		-181-7	-3.87	+0.00	+0.000	+0.000
	TEMP: +		5 (N: 36.				* = =	
0	+498+0				+12.71	+9+1	+476.2	0.6967
ΔID	-398 • 0		-135.6	257.2	-5.21	+0.00	+0.000	+0.000
	TEMP: +8		SXIN: 36.2					
	-519.3	¥ 43• 4		698.5	+13.47		+ 602.2	
	31703	+0•0	-179.8 -	332.9	-6.57		+0.000	

TABLE A-10 (CONCLUDED)

```
RHI
      LAHET
              LHMIN
                      LREGD
                              LHMAX
                                      LHRES
                                              LHDSK
                                                      L.H WSK
                                                              WETLR
      SEHET
              STARE
                      RADHT
                              CONSK
                                      CORES
                                              PMMH G
                                                      CLØSR
 AIR TEMP:
            +0.00
                    SKIN: 31-89 C 35-44 MMHG
      +21.5
              +32.0
                     -339.4
                              +32.0
                                              +13.2
                                     +8.41
                                                       +0.0 +0.0000
      + 78 . 4
               +0.0
                      +30.2
                              + 44.1
                                      +4.12
                                              +0.00
                                                    +3.940 +27.727
 50
      +20.4
              +30-1
                     -339.4
                              +30.1
                                      +8.01
                                              +12.4
                                                       +0.0 +0.0000
      + 79 . 6
               +0.0
                     +30+6
                              +44.7
                                      +4.21
                                              +2.29
                                                    +3.873 +27.647
100
      +19.3
              +28 - 1
                     -339.5
                              +28 - 1
                                      + 7- 61
                                              +11.7
                                                      +6.0 +0.0000
      +80.7
               +0.0
                     +31 • 1
                              +45.3
                                      +4.29
                                              +4.58
                                                     +3.807 +27.567
 AIR TEMP: +15.00
                    SKIN: 32-11 C 35.88 MMHG
  0
      +26.5
              +33.1
                     -143.7
                              +33-1
                                              +17.3
                                      +9.20
                                                      +0.0 +0.0000
      + 73. 4
               +0.0
                     +31.8
                              +39.5
                                      +2.14
                                              +0.00
                                                    +1.884 +12.730
 50
      +22.4
              +27.5
                     -143.9
                              +27.5
                                      +7.90
                                              +14.5
                                                      +0.0 +0.0000
      +77.6
               +0.0
                     +33.6
                              +41.7
                                      +2.29
                                              +6.39
                                                    +1.744 +12.434
100
      +18.2
              +21.9
                     -144-1
                              +21.9
                                      +6.59
                                              +11.6
                                                      +0.0 +0.0000
      +81.8
               +0.0
                      +35.4
                              + 43.9
                                      +2.45
                                            +12.78
                                                    +1 • 614 + 12 • 131
 AIR TEMP: +23.00
                    SKIN: 32-49 C 36-67 MMHG
      +30.7
  n
              +34.0
                     -37.8
                              +34.0
                                     +9.65
                                              +21-1
                                                      +0.0 +0.0000
      +69.3
               +0.0
                      +31.8
                              +36.4
                                     +1.08
                                              +0.00
                                                    +0.782 +5.050
 50
      +22.9
              +24.R
                                     +7.42
                     -38.0
                              +24.8
                                              +15.5
                                                      +0.0 +0.0000
      + 77. !
               +0.0
                      +35.4
                              + 40 • 4
                                     +1.22
                                            +10.53
                                                    +0.625 +4.487
100
      +14.6
              +15.5
                      -35,2
                              +15.5
                                     +5.16
                                              +9.5
                                                      +0.0 +0.0000
      +85.4
               +0.0
                     +39.2
                                            +21.07
                              + 44.7
                                     +1.51
                                                    +0.490 +3.891
 AIR TEMP: +30.00
                    SKIN: 53.71 C 39.26 MMHG
      + 45. 4
                     +45.4 +606.8 +10.06
             +36.2
                                             +25.7
                                                      +9.7 +0.0162
      +54.6
               +0.0
                     +26.3
                             +28·2
                                     +0.15
                                             +0.00
                                                    +0.000 +0.000
      + 45.1
 50
              +22.1
                     +45.1 +361.5
                                     +6.62
                                             +14.5
                                                     +24.0 +0.0677
      +54.9
                             +28.2
               -0.0
                     +26.3
                                     +0.43
                                            +15-91
                                                    +0.000 +0.000
100
      +44.8
               +8.1
                     +44.8 +116.1
                                     +3.11
                                              +3.3
                                                     +38-4 +0-3402
      +55.2
              +0.0
                             +28.2
                     +26.3
                                     +0.73
                                            +31.83
                                                    +0.000 +0.000
 AIR TEMP: +33.00
                   SKIN: 34.56 C 41.17 MMHG
      + 77. 1
             +37.6
                     +77.1 +636.0 +10.24
                                              +25.6
                                                     +41.3 +0.0660
      +22.9
              -0.0
                     +11-3
                             +11.9
                                     -0.25
                                             +0.00
                                                    +0.000 +0.000
 50
             +21.0
      +76.8
                     +76.8 +345.1
                                     +6.13
                                             +12.3
                                                     +58.4 +0.1722
      +23.2
              -0.0
                     +11.3
                             +11.9
                                     +0.07
                                            +18-87
                                                    +0.000 +0.000
100
      +54.2
              +4.2
                     + 76. 4
                             +54.2
                                     +1.92
                                              0.0
                                                    +52-2 +1-0000
      +23.6
             +22.3
                     +11.3
                             +11.9
                                     +0.41
                                            +37.73
                                                    +0.000 +0.000
 AIR TEMP: +37.00
                    SKIN: 35.30 C 42.89 MMHG
    +126.2
             +39+0
                   +126.2 +662.4 +10.48
                                             +24.5
                                                     +91.2 +0.1399
      -26.2
              -0.0
                                             +0.00 +0.000 +0.000
                     -12.5
                            -12.9
                                     -0.78
 50
                    *125·8
    +125.8
             +18.2
                           +299.5
                                     +5.33
                                              + 7.9
                                                    +112.6 +0.3827
     -25.8
              +0.0
                     -12.5
                            -12.9
                                     -0.40
                                            +23.54
                                                    +0.000 +0.000
100
             -63.6
     -63.6
                    +125.4
                            -63.6
                                     +0.00
                                             +0.0
                                                    -63-6 +1-0000
     -25.4 +189.1
                     -12.5
                             -12.9
                                     +0.00
                                           +47.08
                                                    +0.000 +0.000
 AIR TEMP: +45.00
                   SKIN: 35.83 C 44.17 MMHG
             +40.4 +242.1 +682.3 +10.99
    +242.1
                                             +20-1
                                                    +210.9 +0.3142
    -142.1
              +0.0
                     -70 • 6
                            -69.7
                                             +0.00 +0.000 +0.000
                                    -1.85
    +127.9
              +8.5 +241.5 +127.9
                                    +3.05
                                              +0.0 +124.9 +1.0000
    -141.5 +113.6
                            -69.7 -1.32 +35.95 +0.000 +0.000
                     - 70 - 6
AIR TEMP: +50.00 SKIN: 35.96 C 44.48 MMHG
 0
   +319.9
             +40.9 +319.9 +687.4 +11.31
                                             +16.8 +291.8 +0.4316
              +0.0 -110.7 -106.7 -2.52
    -219.9
                                             +0.00
                                                    +0.000 +6.000
    -26.2
            -26.2 +319.3
                            -26.2
                                    +1.06
                                             +0.0
                                                    -27.3 +1.0000
    -219.3 +345.5 -110.7 -106.7
                                    -1.87 +46.28
                                                    +0.000 +0.000
AIR TEMP: +60.00 SKIN: 36.10 C 44.81 MMHG
    +483.5
             +41.8 +483.5 +693.0 +12.00
                                              +9.6 +461.9 +0.6783
              +0.0 -198.0 -181.7 -3.87
    -383.5
                                             +0.00 +0.000 +0.000
AIR TEMP: +70.00 SKIN: 36.16 C 44.97 MMHG
            +42.6 +656.4 +696.2 +12.71
   +656+4
                                              +1.8 +641.9 +0.9391
    -556.4
             +0.0 -294.0 -257.2 -5.21
                                             +0.00
                                                   +0.000 +0.000
AIR TEMP: +80.00 SKIN: 36.20 C 45.06 MM (G
   +698.5 +43.4 +838.5 +698.5 +13.47
                                              +0.0 +685.0 +1.0000
    -738.5 +140.1 -399.1 -332.9 -6.57
                                            +0.00 +0.000 +0.000
```

TABLE A-11

METABOLIC HEAT TRANSFER - PROGRAM LISTING

```
100 REM: > SIMOC5 < 5/72
110
    DIM AS(60), BS(38), CS(34), DS(38), ES(34)
    A5="
                     METABOLIC PARAMETERS WITH OPTIMUM CLOTHING"
120
130
    BS=" RHT
               LAHET
                       LHMIN LREOD
                                       LHMAX"
   C$="
140
          LHRES LHDSK
                          LHWSK
                                   WETLR"
    D$="
150
                SFHET STORE RADHT CONSK"
160
    E$="
           CORES
                  PMMHG
                           CLØSR CLØDT"
    PRINT USING "4(DDD)"; TIM(3), TIM(2), TIM(1), TIM(0)
180
    IMAGE " AIR TEMP:", S3D.DD,"
                                   SKIN:",3D.DD," C ",3D.DD," MMHG"
    IMAGE 4D, XS4D.D, XS4D.D, XS4D.D, XS4D.D, XS4D.D, XS4D.D, XS4D.D, XS4D.D, XSD.4D
200
210
     *44GE 5XS4D.D, XS4D.D, XS4D.D, XS4D.D, XS3D.DD, XS3D.DD, XSDD.3D, XSDD.3D
250
250
    T7=37
270 M=M0=100
280
   A*2
290
    A1=1.9
300
    A2=1.3
310
    J1=4.8
320 H1=4
330 H2= . 35
340
    E1=2*H1
350
    G=.006*M
360 M1=M/A
    PRINT ".";LIN(1);AS
400
410
    PRINT LIN(1);B$;C$
430
    PRINT DSJES
450
    DATA 10,20,25,27,29,31,35,40,52
    DATF. 99
490
510 T6=35.5-.03*M1
520
    IF M1>50 THEN 550
530
    L4=0
540 G 0T 0 560
550
    L4= • 4 + A + (M1 - 50)
    PRINT
560
    READ T
610
620
    IF T>95 THEN 2900
    T3=T6+1.5*ATN(.1967*(T-31))
630
640
    T1=T0=T
650 T9=T3
660
    GUSUB 2610
670
    P3=P9
680
    U0=28+T/10
690
    U=EXP(T+(40819.+132.5+T-.0128+T+3)+.000001)
700
    U1=U0+U
    B1=(T1+273.15)/100
710
720
    B3=(T3+273-15)/100
730
    C3*H1*A1*(T3-T)
740 R3=J1+A2+(B3+4-B1+4)
750
    T9=T
    GØSUB 2610
760
770
    P1=P9
780 PRINT USING 190; T. T3. 760 *P3
790 E4=L4
1010 FOR Y2=0 TO 100 STEP 50
1020
     P=P1+Y2/100
1000 IF (760*P)>56 THEN 2180
1040 P9=P
1050 T9=T
1060 GØSUB 2810
1070 W=W9
```

TABLE A-11 (CONTINUED)

```
1080
     U2#U0+U*Y2/100
1090
     T9=U2
1100
     GØSUB 2610
     G0SUB 2810
1110
     W2=W9
1120
     U3=(T7+U2)/2
1130
1140 H3=597.4-.568+U3
1150 L3=G+(W2-W)+H3
1160 D3=G*(.2403+.216*(W2+W))*(U2-T)
1170
     L7=H2*A1*(P3-P)*760
     L8=E1+A1+(P3-P)+760
1180
1190
     S3=C3+R3+D3
     IF L8 <= L4 THEN 1230
1200
1210
     R4=L4/L8
1220
     GØTØ 1240
1230
     R4=1
     Z2=M0-L3-L7-R4*(L8-L7)-D3
1240
1250
     Z3=C3+R3
     IF Z3>Z2 THEN 1610
1590
1310 K2=D5=0
1320 R1=R3
1330 C1=C3
1340
     S= 53
1350 L6#M0-S
1360 L5=L6-L3
1370 IF L5>L8 THEN 1420
1380
     R5=(L5-L7)/(L8-L7)
1410
      GØTØ 1440
1420
     RS= 1
1440
     L1=R5+L8-L4
1450 L2=(1-R5)*L7
1460
     L=L1+L2+L3+L4
1470
     L0=L3+L7+R4*(L8-L7)
1480 L9=L8+L3
1490 X6=L6-L
1500
     GØTØ 2010
1610
     R5=R4
     L0=L9=L3+L7+R5*(L8-L7)
1620
1630 L6≈M0~S3
1650 N=1
1660 N1=0
1670
     N2=4/N
1680
     FOR K2=N1 TO N1+4NN2 STEP N2
1690
     F2=1+.1*X2
1700 F3=1/(1+.1*K2)
1710
     F4=1/F2
1720
     L2=F3+(1-R5)+L7
1730
     E4=F4+L4
1740
     Z5=M0-L3-D3-E4-L2
17 50
    T2=T3-+18#K2=Z5/A1
     B2=(T2+273.15)/100
1770
1780
     B0=(T0+273.15)/100
1790
     C2=H1+F2+A1+(T2-T)
1800
     R2=J1+F2+A2+(B2+4-B0+4)
1810
     Z4=C2+R2
1820
     IF 24<25 THEN 1840
1830 NEXT K2
1840
     IF N2<.0005 THEN 1880
1850
     N1=K5-N5
1860
     N=2#N
1870
     GØTØ 1670
```

TABLE A-11 (CONCLUDED)

```
1880
      D5=T3-T2
1910
      C1=C2
1920
      R1=R2
1930
      S=C1+R1+D3
1950
      L1=0
1960
      L=L1+L2+L3+E4
1970
      X6=M0-S-L
2010
      E5=L1+E4
      DEF FNR(Q) = (Q/MO) +100
2020
2030
      L=FNR(L)
2040
      S= FNR(S)
2050
      LO=FNR(LO)
2060
      L6=FNR(L6)
2070
     19# FNR(19)
2080
      L3=FNR(L3)
2090
      L2=FNR(L2)
2100
      ES=FNR(ES)
      X6=FNR(X6)
2110
2120
      R1=FNR(R1)
2130
      C1=FNR(C1)
2140
      D3=FNR(D3)
2160
      PRINT
             USING 200; Y2, L, LO, L6, L9, L3, L2, E5, R5
2170
      PRINT
             USING 210; S, X6, R1, C1, D3, 760*P, K2, D5
2180
     NEXT Y2
2190
      G @ T Ø 610
2610
      IF T9<0 THEN 2710
2620
      01=-17.5604
2630
      02=+1.79764
2640
      Q3=+3.86061
2650
      04=-1.41654
2660
      Q6=373.15/(273.15+T9)
2670
      Q7=Q6-1
2680
      08=07/06
      Q9=Q1*Q7+Q2*LØG(Q6)+Q8*(Q3+Q4/Q6)
2690
2760
      G0T0 2780
2710
      Q1=-20.9422
2720
      Q2=-3.57281
2730
      Q3*+2.02115
      Q6=273.15/(273.15+T9)
27 40
2750
      07=06-1
2760
      Q8=Q7/Q6
2770
      Q9*Q1*Q7+Q2*L0G(Q6)+Q3*Q8-5.11145
      P9=EXP(09)
2780
2790
      RETURN
      X9=+62197+P9/(P8-P9)
2810
2820
      IF T9<0 THEN 2860
2830
      90=66-T9
2840
      Q5=1+.004*P8+1/(500+Q0+2)
2850
      GØTØ 2870
      Q5=1+(4200-15*T9+.375*T9+2)*.000001*P8
2860
2870
      C9=(P8-P9)/(P8/Q5-P9)
      W9=C9*X9
2880
2890
      RETURN
2900
      PRINT
      PRINT "
2910
                           MI
                                   MO
                                            Lá
                                                     T6
                                                              Pg"
      PRINT USING "6(XDDDD.DD)";M.MI.MO.L4, T6, P8
2920
      PRINT "
                           A2
                                            HI
2930
                  A1
                                   J١
                                                     E 1
      PRINT USING "6(XDDDD.DD)";A1,A2,J1,H1,E1,G
29 40
      PRINT " T3=34+1.5*ATN[0.1967+(T-31)] U0=28+T/10"
2950
      PRINT " VI= "1.00925*H1+2;"M/S ";1.82*H1+2;"FPM"
2970
      PRINT " TI=TO=T F2=1+.1+K2 F3=1/(1+.1+K2)"JLIN(1)
2980
300n
      END
```

Appendix B

TABULATED DATA RELATING TO PARTIAL RECIRCULATION OF AIR

The salient results of the study relating to partial recirculation of ventilating air in shelters during cold weather are shown in graphic form on Figures 7 and 8 in Section III, Shelter Ventilation. Tables B-1 through B-5 represent data used for preparation of Figure 8, as well as some parameters that are not shown graphically. All of these tables relate to a recirculating system during winter operation with a minimal mixture temperature of 50°F (i.e., the temperature of air supplied to occupied spaces is 50°F). The data therefore apply when the fresh or outside air temperature is 50°F or less. Each table is based on a single value of fresh air temperature as indicated on the first tabulated line, along with WSAT, which is the humidity ratio of saturated air at the fresh air temperature. The first column in each table shows the two values for relative humidity of fresh air, Y1 = 0 or 100 percent, used in the computations. In each of the other six columns there are values of two quantities for each value of relative humidity, as indicated by the upper and lower symbols at the head of each column. In column 2, SCFM2 is the total ventilating capacity or mixed air quantity, V2, in SCFM per person, and V2CFM is the mixed air volume corrected to actual conditions of temperature and humidity. In column 3, SCFM1 is the flow rate of fresh air in SCFM per person, and SCFM4 is the flow rate of recirculated air in SCFM per person. In column 4, T3 (F) is the dry bulb temperature and DOPT3 is the dew point of air that is either recirculated or exhausted to the atmosphere. In column 5, MAIRW2 is the humidity ratio of mixed air, and RAIRW3 is the humidity ratio of air that is either recirculated or exhausted. In column 6, VI/V2 is the ratio of fresh to total air flow quantities. The difference, W3 - W1, is the increase in humidity ratio of air passing through the system, that is, the increase from outside to exhaust conditions. In column 7, DH/DW is the slope of the mixing process line in the coordinate system of specific enthalpy and humidity ratio. The quantity, LBW/DAY, is the amount of water added to the ventilating air by metabolic processes in pounds per day per person. Data relating to partial recirculation of ventilating air in shelters, as shown in these tables and plotted in Figure 8, were computed with the BASIC program listed in Table B-6.

TABLE B-1

PARTIAL RECIRCULATION OF VENTILATING AIR MIXED AIR TEMPERATURE = 50 °F FRESH AIR TEMPERATURE = 50 °F

RH 1	SCFM2	SCF41	T3(F)	MAIRW2	V1/V2	DH/DW
	V2CF4	SCFM4	DØPT3	RAIRWS	W3-W1	LBWDAY
	•••					
FRES	H AIR T	E4P# +50	0.00 F. W	SAT= 0.007	659	
0	60.00	60.00	+54.58	0.000000	1.00000	4222.0
	57.83	0.00	-14.90	0.000351	0+000351	2.274
100	60.00	60.00	+54.52	0.007659	1.00000	4222.0
	58 • 5 4	0.00	+51 • 18	0.008009	0.000351	2.274
0	40.00	40.00	+56.87	0.000000	1 • 00000	4228.0
	38 • 55	0.00	-7.54	0.000526	0.000526	2.274
100	40.00	40.00	+56•78	0.007659	1.00000	4222.0
	39.03	0.00	+51 • 76	0.008185	0.000526	2.274
0	30.00	30.00	+59.16	0.000000	1.00000	4222.0
	28.91	0.00	-2.17	0.000702	0.000702	2.274
100	30.00	30.00	+59+03	0.007659	1.00000	4222.0
	29.27	0.00	+52+33	0.008360	0.000702	2.274
0	50.00	20.00	+63.73	0.000000	1.00000	4222.0
	19.28	0.00	+5.61	0.001053	0.001053	2.274
100	50.00	20.00	+63.54	0.007659	1 • 00000	4222.0
	19.51	0.00	+53-44	0.008711	0.001053	2.274
0	15.00	15.00	+68 • 29	0.000000	1.00000	4222.0
	14.46	0.00	+11.30	0.001404	0.001404	2.274
100	15.00	15.00	+68+04	0.007659	1.00000	4222.0
	14.63	0.00	+54.51	0.009062	0.001404	2.274
0	10.00	10.00	+77-40	0.000000	1.00000	4222.0
	9.64	0.00	+19.55	0.002105	0.002105	2.274
100	10.00	10.00	+77.03	0.007659	1.00000	4222.0
	9.76	0.00	+56-53	0.009754	0.002105	2.274
0	7.00	7.00	+87 - 58	0.000000	1.00024	3804•6
	6.75	-0.00	+29.24	0.003335	0.003335	2 • 521
100	7.00	7.00	+87-26	0.007659	1.00050	355ë• 4
	6.83	-0.70	+59 • 68	0.010951	0.003292	2 • 489
0	5.00	5.00	+92.79	0.000000	0.99962	2611.2
	4.82	0.00	+46.91	0.006911	0.006811	3.678
100	5.00	5.00	+92.66	0.007659	G•99996	2651.3
	4.88	0.00	+67-25	0.014364	0.006706	3.621
0	3.00	3.00	+94.86	0.000000	0•99993	1733.0
	2.89	0.00	+72.23	0.017099	0.017099	5.540
100	3.00	3.00	+94.95	0.007659	0.99330	1746.5
	2.93	0.00	+82.91	0.024626	0.016967	
0	8.00	2.00	+95.00	0.000000	1.00024	1457-2
	1.93	-0.00	+99+33	0.030492	0.030492	
100	5.00	VS T33	L3W, 830			1 463 • 8
100	2.41	2 • 41	+94.97	0.007659	1.00000	1563 • 4
	2.35	0.00	+90+01	0.031184	0.023526	6.121

PARTIAL RECIRCULATION OF VENTILATING AIR MIXED AIR TEMPERATURE = 50 °F FRESH AIR TEMPERATURE = 40 °F

TABLE 8-2

RHI	SCF42	SCF41	T3(F)	441RW2	V1/V2	DH\OM
	VSCF4	SCF44	DØPT3	RATRWS	W3- W1	LBW/DAY
	•					
FRES	H AIR T	E4P= +40	.00 F. WS	SAT= 0.005	213	
0	60.00	13.86	+54.59	0.000765	0.31433	4222.0
•	57.90	41 - 14	+6.76	0.001116	0.001116	2.274
100	60.00	18 - 74	+54-53	0.005986	0.31231	4222.0
• • • •	58 • 39	41.26	+45.02	0.006337	0.001124	2.274
0	40.00	16.30	×56.36	0.000765	0 - 40 746	4222.0
•	35 • 60	23.70	+9.65	0.001292	0.001292	2.274
100	40.00	16.21	+56+80	0.005986	0 - 40519	4222.0
	38.92	23.79	+45.73	0.006512	0.001299	2.274
0	30.00	14.35	+59.14	0.000765	0.47332	4222.0
•	28.95	15.65	+12-19	0.001467	0.001467	2.274
100	30.00	14.28	+59 • 0 6	0.005986	0-47597	4222.0
100	29 • 19	15.72	+ 46 • 43	0.006638	0.001474	2.274
0	20.00	11.58	+63.71	0.000765	0.57900	4222.0
•	19.30	8 42	+16.53	0.001818	0.001818	2.274
100	20.00	11.53	+63-59	0.005996	0.57670	4222.0
100	19.46	8 47	+47.77	0.007039	0.001825	2.274
0	15.00	9.71	+68.27	0.000765	0.64711	4222.0
U	14.47	5.29	+20-16	0.002169	0.002169	2.274
100	15-00	9.67	+63.09	0.005986	0.64496	4222.0
100	14.60	5.33	+49.06	0.007390	0.002176	2.274
0	10.00	7.33	♦ 77•36	0.000765	0.73338	4222.0
U	9.65	2.67	+26.04	0.002871	0.002871	2.274
100	10.00	7.32	+77-11	0.005986	0.73153	4222.0
100	9.73	2.69	+51.47	0.003736	0.002878	2.274
O	7.00	5.54	+87.55	0.000371	0.79103	3813.8
U	6.76	1 • 46	+34.62	0.004209	0.004209	2.520
100	7.00	5.53	+97.33	0.006937	0.79013	3848 • 2
100	6.81	1.47	+55.47	0.009390	0.004176	
0	5.00	4.06	+92.76	0.007570	0.81296	2621.0
U	4.53	0.94	+52.29	0.008343	0.008343	
.00		4.06	+92.67	0.006759	0.31285	2648 • 6
100	5.00		+65.44	0.003737	0.008258	3. 625
0	4 · 8 7 3 • 00	0•94 2•47	+94.85	0.003658	0.82340	1739.8
U	2.91	0.53	+77.75	0.020693	0.020693	
100	3.00	V2 T30	Law. Fag		AIR	1748.8
100		3-16	+94.30	0.007659	0.81949	2075.0
100	3.86		+74.70	0.018762	0.013548	
^	3.77	0 • 70				
0	2.00	VS TOO	LOW, ROD			1462 • 6
0	2.26	1.87	+94.98	0.005420	0.82616	1526.3
	2.20	0.39	+90+01	0.031179	0.031179	
100	2.00	V2 T00	LOW, BOD		RAGE	1467.3
100	2.57	V2 T00	Law. Fog			1615.8
100	3.86	3-16	+94.30	0.007659	0.81949	2075.0
	3.77	0 • 70	+74+90	0.018762	0.013548	4• 628

TABLE 8-3

PARTIAL RECIRCULATION OF VENTILATING AIR MIXED AIR TEMPERATURE = 50 °F FRESH AIR TEMPERATURE = 20 °F

RH 1	SCF42	SCFY1	T3(F)	MAIRW2	87 / IV	DH/DW
	V2CF4	SCF44	DØPT3	R41RW3	W3- W1	LBW DAY
FRES	H AIR T	EMP= +20	0.00 F. WS	SAT= 0.002	1 52	
0	60.00	7•95	+54.56	0.002296	0.13256	4222.0
	59 • 0 4	52.05	+24.33	0.002647	0.002647	2.274
100	60.00	7.93	+54.54	0.004457	0.13211	4222.0
	58.24	52.07	+37.95	0.004808	0.002656	2.274
0	40.00	7.46	+56,84	0.002296	0.18647	4222.0
	34 • 69	32.54	+25.69	0.002823	0.002323	2.274
100	40.00	7.44	+56.31	0.004457	0.18588	4222.0
	38 • 83	32.56	+38+86	0.004993	0.002832	2.274
0	30.00	7.02	+59.12	0.002296	0.23408	4222.0
	29.02	22.98	+26.97	0.002998	0.002993	2.274
100	30.00	7.00	+59 • 08	0.004457	0.23339	4222.0
	29.12	23.00	+39 • 73	0.005159	0.003007	2.274
0	20.00	6.29	+63.67	0.002296	0.31433	4222.0
	19.35	13.71	+29.34	0.063349	0.003349	2.274
100	20.00	6.27	+63.62	0.004457	0.31349	4222.0
	19.41	13.73	+ 41 - 41	0.005510	0.003358	2.274
0	15.00	5 • 69	+68.22	0.002296	0.37936	4222.0
	14.51	9.31	+31 • 49	0.003700	0.003700	2.274
100	15.00	5 • 68	+68-14	0.004457	0.37844	4222.0
	14.56	9.32	+43.00	0.005861	0.003709	2.274
0	10.00	4.78	+77.29	0.002296	0.47832	4222.0
	9.67	5.22	+35.73	0.004402	0.004402	2.274
100	10.00	4.77	+77.18	0.004457	0.47734	4222.0
	9 - 71	5.23	+45.94	0.006563	0.004411	2.274
0	7.00	3.91	+87.48	0.002619	0.55829	3828 • 1
	6.77	3.09	+43.36	0.005942	0.005942	2.512
100	7.00	3.90	+87.38	0.004766	0.55782	3843.4
	6-80	3.10	+51 • 41	0.009075	0.005223	2 • 501
0	5.00	2.96	+92.71	0.004630	0.59271	2638.0
	4.85	2.04	+60 • 71	0.011370	0.011370	3+640
100	5.00	2.96	+92.67	0.006767	0.59246	2649.0
	4.97	2.04	+65.45	0.013479	0.011327	3 • 625
0	3.00	V2 TØ3	LOW, FOG	IN MIXED	AIR	1752.5
0	3.74	2.26	+94.41	0.007659	0 • 60514	2024.2
	3.65	1 • 49	+75.87	0.019396	0.019396	4.743
100	3.00	VS TOO	L3W. FØG	IN MIXED	AIR	1756-1
100	4.54	2 • 71	+93+46	0.007659	0.59747	2397.1
	4.43	1.93	+70.01	0.015930	0.013678	4.004
0	2.00	V2 T00	LOW. BOD	Y HEAT ST	BRA GE	1472.9
0	2.77	V2 T30	LOW. FOG	IN MIXED	AIH	1679.3
0	3.74	2.26	+94.41	0.007659	0.60514	2024.2
	3.65	1 • 48	+75.87	0.019396	0.019396	4.743
100	2.00	V2 T00	LOW, BOD		RA GE	1475.0
100	2.90	V2 T00		IN MIXED		1724.7
100	4.54	2.71	+93.46	0.007659	0.59747	2397.1
	4.43	1.83	+70.01	0.015930	0.013678	4.004
						'

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TABLE 8-4

PARTIAL RECIRCULATION OF VENTILATING AIR MIXED AIR TEMPERATURE = 50 °F FRESH AIR TEMPERATURE = 0 °F

RHIL	SCFM2	SCFM 1	T3(F)	YAIRW2	V1/V2	PH\D.A
	V2CFM	SCF44	D3PT3	RAIRWS	W3- W1	LEW/DAY
FRES	H AIR	14P=	+0.00 F. V	SAT= 0.00	10.78.7	
0	60.00	5.04		0.003827		4000 0
•	58 - 18	54.96	+34-42	0.003327		4222.0
100	60.00	5.03	+54.54			2.274
	58.26	54.97		0.004620		4222.0
0			+39 • 79	0.004971		2.274
U	40.00	4.84	+56-82	0.003827		4222.0
4.00	38.79	35-16	+35.45	0.004353		2.274
100	40.00	4.83	+56.81	0.004620	0.12075	4222.0
_	13.84	35.17	+39.67	0.005146	0.004359	2.274
0	10.00	4-65	+ 59 • 09	0.003827	0.15496	4222.0
	29.09	25.35	+36.44	0.004529		2.274
100	30.00	4.64	+59+08	0.004620		4222.0
	29.13	25.36	+40+53	0.005321	0.004534	_
0	20.00	4.31	+63-63	0.003827	0.21572	2.274
	19.39	15-69	+ 38 - 32	0.004880		4222.0
100	20.00	4.31	+63-61			2.274
	19.42	15.69		0.004620	0.21549	4222.0
0	15.00	4.03	+42-16	0.005672	0.004885	2.274
•	14.55		+68+16	0.003827	0-26934	4222.0
100	_	10.97	+40.09	0.005231	0.005231	2.274
100	15.00	4.02	+68.14	0.004620	0.26805	4222.0
_	14.56	10.98	+ 43 • 71	0.006023	0.005236	2.274
0	10.00	3.55	+77.21	0.003927	0 > 35489	4222.0
	9.70	6•4 5	+43.32	0.005932	0.005932	2.274
100	10.00	3.55	+77.17	0.004620	0.35456	4222.0
	9.71	6.45	+ 46 • 59	0.006725	0.005938	2.274
0	7.00	3.02	+87.41	0.004349	0.43157	
	ۥ 79	3.98	+50.01	0-007662		38 40 • 2
100	7.00	3.02	+87.38	0.005136	0.007662	2.504
	6.80	3.99	+ 52 • 62		0 • 43125	3544.2
0	5.00	2.33		0.008447	0.007660	2.50
	4.88	2.67	+92.66	0.007649	0.46692	2652•6
100	5.00		+67.23	0.014354	0.014354	3. 621
100	5.31		LOW, FOG	IN MIXED	AIR	2656.3
.00		2.45	+92.02	0.007659	0.46242	2833.9
0	5-18	2.85	+65.64	0.013572	0.012785	3 • 38 9
	3.00	CET SV	LOW. BODY	HEAT ST	RAGE	1764.5
0	3.50	RET SV	LØW, FØG		AIR	1832.6
0	5.00	5.33	+93.66	0.007659	0 • 46650	2651 • 6
	4.88	2.67	+67.25	0.014364	0.014364	3 • 621
100	3.00	VS T33	LOW, BODY	HEAT STO	RAGE	1766-2
100	3.25	V2 TØÐ	LØW. FØG	IN MIXED	ATR	1852.3
100	5.31	2 • 45	+92.02	0.007659	0 • 462 42	
	5.18	2.85	+65.64	0.013572	0.012785	2933.8
0	2.00	CET SV	Law. Bady			3 • 389
ō	3.20	VS TOO				1483.2
Č	5.00	2.33	+92-66		AIR	1832-6
_	4-88	2.7		0.007659	0 • 46680	2651.6
100	5.00		+67.25	0.014364	0.014364	3 • 621
100		V2 700	LOW BODY		RA GE	1483.8
	3.25	V2 TØØ	LOW, FOG	DEXIP VI	AIR	1852.3
100	5.31	2.45		0.007659	0 • 46242	2833.8
	5.18	2.85	+65.64	0.013572	0.012785	3 • 339

TABLE B-5

PARTIAL RECIRCULATION OF VENTILATING AIR MIXED AIR TEMPERATURE = 50 °F FRESH AIR TEMPERATURE = -20 °F

RH1	SCFM2	SCFMI	T3(F)	MAIRW2	V1/V2	UHZDW
	VSCFY	SCFM4	DØPT3	RAIRW3	M3- M1	LBW/DAY
	14.0.	20	501.44			
FDF6	U A 2 3 T	.can-	0.00 F. W	SAT= 0.000	1262	
0	60.00	3.69	+54.54	0.005358	0.06147	4222.0
3		56.31	+ 42 • 31		0.005709	
100	58 • 33			0.005709		2.274
100	60.00	3,69	+54.54	0.005623	0.06144	4222.0
_	58 • 35	56.31	+ 43 • 50	0.005974	0.005711	2.274
0	40.00	3 • 58	+56+80	0.005358	0.08945	4222.0
	38 • 88	36• 42	+43-11	0.005884	0.005884	2.274
100	40.00	3•58	+56+80	0.005623		4222.0
	38•90	36•42	+44.25	0.006150	0.005887	2.274
0	30.00	3•47	+59+07	0.005358	0.11581	4222.0
	29.16	26.53	+ 43 • 87	0.006060	0.006060	2.274
100	30.00	3.47	+59+06	0.005623	0.11576	4222.0
	29 • 18	26-53	+44.98	0.006325	0.006068	2.274
0	20.00	3.28	+ 63 • 59	0.005358	0 - 1 6 4 2 1	4222.0
	19.44	16.72	+ 45 - 33	0.006411	0.006411	2.274
100	20.00	3.28	+63.59	0.005623	0.16414	4222.0
	19.45	16.72	+ 46 - 39	0.006676	0.006413	2.274
0	15.00	3.11	+68.12	0.005358	0.20758	4222.0
•	14.58	11.89	+ 46 • 72			
100	-			0.006762	0.006762	2.274
100	15.00	3.11	+68-11	0.005623	0.20751	4222.0
_	14.59	11.89	+ 47. 73	0.007027	0.006764	2.274
0	10.00	5.85	+77-14	0.005358	0.28210	4222.0
	9.72	7-18	+ 49 • 32	0.007463	0.007463	2.274
100	10.00	2.88	+77-13	0.005623	0.58500	4282.0
	9•73	7.18	+50+25	0.007729	0.G07466	2.274
0	7•00	2• 46	+87+33	0.006066	0.35188	3851.8
	6.91	4.54	+ 55 • 41	0.009369	0.009369	2 • 49 7
100	7.00	2.46	+87+33	0.006332	0.35171	3951.9
	6.82	4.54	+56.17	0.007636	0.009373	2.493
0	5.00	V2 TOO	LBW, FØG	GEXIM VI	AIR	2667.3
0	6.02	8.83	+90.26	0.007659	0.37035	3279 • 1
	5.87	3 • 79	+62.57	0.012168	0.012168	2.931
100	5.90	V2 T03	LOW. FOG	OBXIN VI	AIR	2671.7
100	6.15	2.26	+99,90	0.007559	0+36789	3353.3
	6.00	3.59	+62-11	0.011962	0.011699	2.358
0	3.00	V2 T33	LOW BEDY		RASE	1776.9
ŏ	3.57	V2 T03				-
ŏ	6.02			IN MIXED		1984.5
0	_	2.23	+90+26	0.007659	0.37035	3279.1
	5.87	3 • 79	+62 • 59	0.012163	691810.0	2.931
100	3.00	V2 T00	LOW BODY			1777.2
100	3.59	VS TOO	LOW, FOG		- •	1992.4
100	6-15	5.56	+89•90	0.007659	0.36739	3358•3
	6.00	3.59	+62-11	0.011962	0.011699	2.859
0	5.00	V2 T33	LOW, BODY	HEAT ST	FRA GE	1493.2
0	3.57	V2 T00	LØW, F3G	DEXIM NI	AIR	1984.6
0	6.02	2.23	+90.26	0.007659	0.37035	3279.1
	5.87	3.79	+62.59	0.012168	0.012163	2.931
100	2.00	V2 T00			RAGE	1493.2
100	3.59	V2 T30		IN MIXED		1992.4
100	6.15	2.26	+89.90	0.007659	0.36739	3358.3
	6.00	3.89	+62-11	0.011762	0.011699	2.359
	0.00	J-1,,	OUTI	0.011706	3-311077	C+ 272

TABLE B-6

RECIRCULATION OF 41R - PROGRAM LISTING

```
1 00
      REMS > RAVENS < 4/72
      PRINT USING "4(DOD)"; TIM(3), TIM(2), TIM(1), TIM(C)
 110
 120
      DIM ASC 481, CSC 601, DSC 601, ESC 501
      A $="
 130
                         PARTIAL RECIRCULATION OF AIR"
      C$=" RH1 SCFM2 SCFM1
 1 40
                                   T3(F)
                                            MAIRWE
                                                        V1/V2
                                                                  D4/DW"
      D$="
 1 50
                 V2CFM SCFM4
                                   DOPT3
                                            RAIR W3
                                                        M3- M1
                                                                 LBW/DAY"
      IMAGE 16X, "MIXED AIR TEMP =", 3D, " F"
IMAGE " FRESH AIR TEMP=", S3D. DD, " F, WSAT= ", D. 6D
 1 60
 170
 180
      IMAGE X3D. X3D. DD. X3D. DD. XXS3D. DD. XXD. 6D. XXD. 5D. XX5D. D
 190
      IMAGE 5X3D.DD, X3D.OD, XX53D.DD, XXD.6D, XXD.6D, XXDD.3D
 200
      IMAGE X3D, X3D, DD, XX, 24, 104, 214, XX5D, D
210
      P8=1
220
      C=+24026
230
      41=1061-09
240
      A2=1061.25
250
      B1=.4412
260
      92= . 4362
270
      93= - 5509
280
      T0=82.5
290
      S0= 4222
300
     40=400
      DATA 20
310
320
      DATA 60, 40, 30, 20, 15, 10, 7, 5, 3, 2
350
      T2=50
360
      T7=90
370
     CO=C*TO
380
     G0=42+82*T0
390
      C2=C*T2
400
      G2=A2+82*T2
410
      T9=(T2-32)/1.9
420
      G73UB 2610
      G85UB 2810
430
440
      S2= W9
450
      T9=(T7-32)/1.9
     G#SUB 2610
460
470
      G# SUB 2810
OFA
     L3= W9
470
     DATA 890,890
500
     D=00=01=.01
510
     ES="TIVE TOO LOW. FOG IN MIXED AIRBODY HEAT STORAGE"
520 PRINT "."ILIN(2) AS
530 PRINT USING 1691T2
     PRINT LINCIDICS:LINCIDIOS
5 40
550
     PRINT
560
     READ TI
     IF TI>TE THEN 1210
570
580
     C1=C*T1
590
     IF TIKE THEY 620
600
     G1=A2+B2*T1
610
     G2 T3 630
620
     G1=A1+B1+T1
630
     T9=(T1-32)/1+8
6 40
     68 SUB 2610
650
     G8 SUB 2810
660
     S1=W9
670
     PRINT USING 170; T1, S1
680
     READ V2
690
    IF V2>404 THEN 2910
     IF V2>303 THEY 520
700
    IF V2>202 THEN 550
710
```

TABLE B-6 (CONTINUED)

```
720 D5=40/(4.5*V2)
730
     Y1=0
740 G3T3 760
750 Y1=100
760
     W1=S1*Y1/100
770
     41=C1+G1 * W1
     W2=(W1*(S0-G1)+C2-C1)/(S0-G2)
730
790
     IF W2>(S2+.00001) THEN 1190
800
     H2=C2+G2*W2
510
     WO=(W2*(SO-G2)+CO-C2)/(SO-GO)
820
     H0=C0+G0+W0
830
     VO=40/(4.5*(HO-H2))
940
     1=11=1
     IF VO>V2 THEY 910
950
867
     H3=42+D5
870
     W3=W2+D5/S0
     T3=(H3-A2*W3)/(C+B2*W3)
830
890
     S=S0
900
     G3T9 1000
910
     H2=C2+G2*W2
920
     ≺3=42+05
930
     G8SUB 15:0
940
     IF 4>3 THEN 1000
950
     S=(H3-H1)/(W3-W1)
960
     X2=(W1*(S-G1)+C2-C1)/(S-G2)
     IF ABS(X2-W2)<(D1/1000) THEN 1000
970
980
     MS=X5
990
     G7T8 910
1000
     V5=V2
1010
      IF W3>L3 THEN 1410
1020 IF W2>(S2+.00001) AND T1<T2 THEN 1310
1040
      T= 459 . 67+ T2
     U2=.001891*V5*T*(1+1.6679*W2)/P8
1050
      D4=43-H1
1060
      V1=40/(4.5*D4)
1070
1080
      R= V1/V5
1090
      V4=V5-V1
      G3 SUB 2260
1100
      43=4.5#V5#(W3-W2)
1110
1120 PRINT USING 1801Y1, V5, V1, T3, W2, R, S
1130 PRINT USING 1901U2, V4, T5, W3, W3-W1, 24*M3
1130
      G2T3 1240
1190
      PRINT USING 200; Y1,-11.11, E$(1,2), E$(5,14), E$(15,30), SO
      IF Y1×40.9 THEN 1250
1200
1210
      READ V2
1 530
      IF V2<202 THEN 1210
1230
      G3T0 690
      IF Y1<49.9 THEN 750
1240
1250
      G3T3 680
1310
      V=3
      PRINT USING 2001Y1, VS, ESC 3, 41, ESC 5, 141, ESC 15, 301, S
1 320
1330
      W2=52
      H2=C2+G2*W2
1340
1350
      S=(42-41)/(W2-W1)
      G95UB 1510
1360
1390
      G3T9 1040
1410
      V=2
1 420
      PRINT USING 200: Y1, V2, ESC 3, 41, ESC 5, 141, ESC 311, S
1 430
      12=91
      G7SUB 1520
1 440
1 460
      G3T3 1020
```

TABLE B-6 (CONTINUED)

```
1510 V2=T0
1520
      ¥4=95
      D1=00
1530
1540
      V1=0
      T3=(N2+N4)/2
1550
      V1=V1+1
1560
      C3=C*T3
1570
      G3=42+B2*T3
1590
1590
     GOTO N OF 1660,1630,1600
1600 X3=(W1*(S-G1)+C3-C1)/(S-G3)
     43=C3+G3*Y3
1610
1620
     G8T3 1660
1630
      K3=C3+G3*L3
1640
      S=(43-H1)/(L3-W1)
1650
      W2=(W1*(S-G1)+C2-C1)/(S-G2)
     IF NI>15 THEN 1790
1660
1670
      WO=(W2*(S0-G2)+C0-C2)/(S0-G0)
1680
      R1=(95-T0)/(95-T3)
     R2=(2305-2+T0)/(2305-2+T3)
1690
1700
     F2=R2*(R1/R2)+.006944
1710
      W3=F2*(B3+W0)-B3
1720
      H3=C3+G3+W3
1730
      IF ABS(H3-K3)<D1 THEN 1850
      IF H3>43 THEN 1770
1740
1750
      12=T3
      G3T3 1550
1760
1770
      V4=T3
      G3T3 1550
1730
1790
      IF D1>.011 THEN 1860
1800
      D1=2*D1
1810
      IF 01>0 THEN 1830
1820
      G3T2 1840
1930
      D=D1
1840
      G2T3 1540
1850
      G2T3 N 3F 1940,1920,1930
      G3TØ N 3F 1950,1900,1870
1860
1870
      W3=X3
1880
      H3=43
1890
      G3T3 1930
1900
      W3=L3
1910
      H3=43
      H2=C2+G2*W2
1920
      V5=M0/(4.5*(H3-H2))
1930
1940
      RETURN
1950
      23=G3-G2
1960
      7.4=C3-H1
1970
      75=D5-C3+C2
1990 Z2=Z3+G3
1990
     Z1=(G2*D5+Z3*Z4-Z5*G3)/Z2
2000
     70=(G2*D5*W1+74*75)/72
2010
      W3=(SOR(Z1+2+4+70)-Z1)/2
2020
      H3=C3+G3*W3
2030
      S=(H3-H1)/(W3-W1)
      W2=(W1+(S-G1)+C2-C1)/(S-G2)
2040
2050
      N=4
2060
      RETURN
5540
      W9=W3
2270
      GØSUB 2510
2280
      P3=P9
```

TABLE B-6 (CONCLUDED)

"H1" ==

```
2290 T9=0
2300 GØSUB 2610
     IF P9>P3 THEN 2340
2310
2320 J1=J=1
2330 G9T9 2350
2340
     J1=J=-1
2350
     J2=0
2360
      J3=32/J1
      FOR T9=J2 T3 J2+3*J3 STEP J3
2370
2380
      G8 SUB 2610
     J6=J+(P9-P3)
2390
2400 IF J6=0 THEN 2470
2410 IF J6>0 THEN 2430
2420
      VEXT T9
2430 IF ABS(J3) <- 005 THEN 2470
2440
      J2=T9-J3
2450
      J1=2*J1
2460
      GØTØ 2360
2470 T5=32+1.8*T9
2480
      RETURN
2510
      F9=P8 + W9/( • 62197+ W9)
2520 IF T9<0 THEN 2560
2530
      20=66-T9
      Q5=1+,004*P8+1/(500+Q0+2)
2540
2550
      GØ TØ 2570
      Q5=1+(4200-15+T9+.375+T9+2)*.000001*P8
2560
2570 P9=F9/Q5
2580 RETURN
2610 IF T9<0 THEN 2710
2620 31=-17-5604
2630 Q2=+1.79764
2640 93=+3.86061
2650 94=-1-41654
2660
      96=373.15/(273.15-T9)
2670 97=96-1
2680 09=07/06
2690 99=91+07+02+L26(06)+05+(93+04/96)
2700 G3T3 2780
2710
      01=-20-9422
2720
      02=-3.57281
2730
      93=+2.02115
2740
      Q6=273.15/(273.15+T9)
2750
      97=96-1
2760 08=97/96
2770 99=01*97+92*L06(96)+93*98-5-11145
2780 P9=EXP(99)
2790
      RETURN
      X9=+621974P9/(PR-P9)
2810
2820 IF T9<0 THEY 2860
2830
      Q0=66-TS
      95=1+.004*P8+1/(500+90+2)
2840
2850
      GO TO 2870
      Q5=1+(4200-15+T9+.3759T9+2)+.000001*P8
2860
      C9=(P8-P9)/(P8/Q5-P9)
2870
2880
      W9=C9*X9
      RETURY
2890
2910
      PRINT
      PRINT " LHR=.25 (T<82.55.T) LHR=.06*T-4.7"
2940
2980
      PRINT USING "2(30). 3X, 40, 2(40.00)"; TIM(1), TIM(0). NO. 01. 0
3000 END
```